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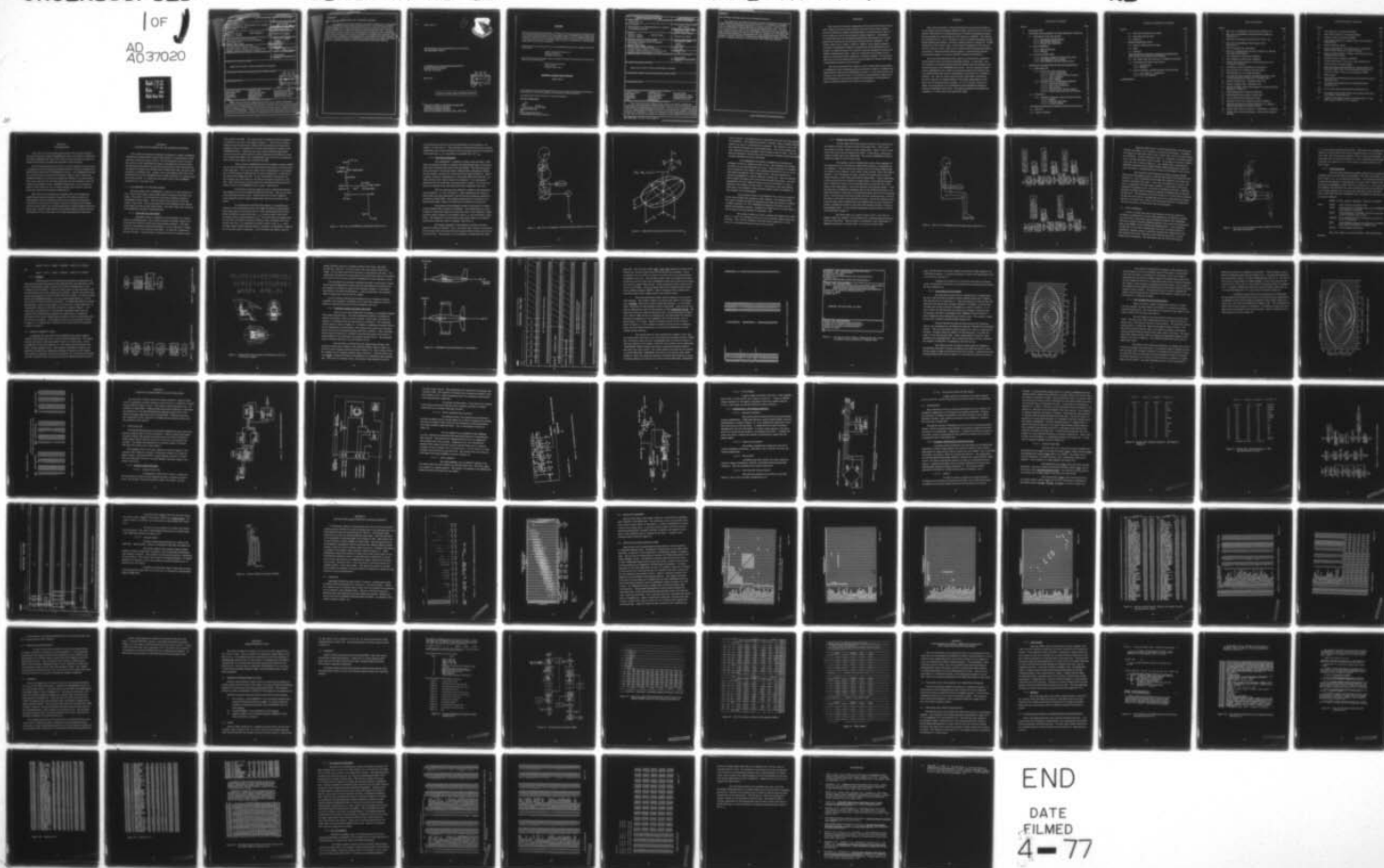
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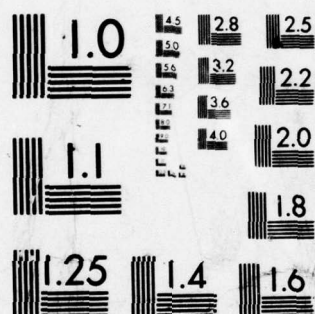
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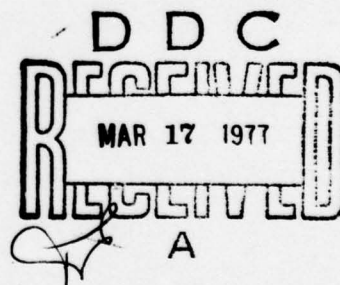
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**BIOMECHANICS AND ANTHROPOMETRY FOR COCKPIT
AND EQUIPMENT DESIGN**

**UNIVERSITY OF DAYTON RESEARCH INSTITUTE
BIOENGINEERING DIVISION
DAYTON, OHIO 45469**

March 1976



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**AEROSPACE MEDICAL RESEARCH LABORATORY
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AIR FORCE SYSTEMS COMMAND
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FOR THE COMMANDER



CHARLES BATES, JR.

Chief

Human Engineering Division
Aerospace Medical Research Laboratory

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and obtaining visibility plots of the workstation boundary.

The report also documents technical procedures followed in readying the AMRL HERCULES (Human Engineering Research to Cull Efficient Strength) Lab for measuring strength capabilities of seated operators, and the procedures established for running the subjects and gathering the data. The last area covered in this report is the development of programs and the manipulation of anthropometric data used in the analysis of human size variability data. This includes preliminary documentation for the Multiple Bivariate Plotting program, and the procedure established in standardizing the AMRL Data Bank Library Computer Programs, and the AMRL Data Bank Tape Library.

SUMMARY

This report describes the engineering services performed by the University of Dayton Research Institute (UDRI) to provide the Aerospace Medical Research Laboratory (AMRL) with biomechanic and anthropometric data in a form readily and clearly interpretable by design engineers. The ultimate use of the data will be in developing specifications and standards for cockpit geometries of advanced aircraft and personal-protective equipment. The primary effort was to modify, maintain, validate, and document computer programs for guiding the design and evaluation of cockpit geometries and to present, in standard format, the computer programs designed for analyses of military anthropometric data. These are required for the design of workstations, personal-protective equipment, and human analogs. The secondary effort was to provide engineering and research support to studies describing strength characteristics of AF personnel.

The work described in this report is a direct outgrowth and represents a continuation of the development and documentation of AMRL's COMPUTERIZED BIOMECHANICAL MAN-model (COMBIMAN) program. It also describes the continuation of the extensive work in developing and standardizing computer programs designed for the efficient analysis of presentation of anthropometric data for guiding the design of AF systems and equipment.

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PREFACE

This report documents research performed by personnel of the University of Dayton Research Institute (UDRI) for USAF Contract F33615-75-C-5092, entitled "Biomechanics and Anthropometry for Cockpit and Equipment Design". The government work unit number for this contract is 71840824. The contract was monitored by Dr. Joe W. McDaniel, of the Crew Station Integration Branch, Human Engineering Division, Aerospace Medical Research Laboratory, Wright-Patterson Air Force Base, Ohio. The principal investigator on the contract was Ms. Susan M. Evans, while Paul E. Kikta provided programming support, and Martin J. Himes provided technical support. David Nearing provided programming support for program RANDM, documented in Section 3.

The research documented in this report was performed in conjunction with personnel of the Crew Station Integration Branch. In particular, Drs. Joe McDaniel and Kenneth Kennedy provided valuable data and equations used in the generation of the COMBIMAN man-model. The link system presently used in COMBIMAN is the result of research performed by personnel in the Crew Station Integration Branch (AMRL/HED), in particular Dr. Kenneth W. Kennedy. Mr. Charles Clauser directed much of the effort involving the bivariate program, the standardization of the AMRL Anthropometric Data Base, and the biostereometric program. Dr. H. E. Krause, formerly of UDRI, also participated in the development of the enfleshment ellipsoids about the COMBIMAN man-model. The authors gratefully acknowledge his assistance, as well as that of the staff of the UDRI.

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SECTION 1

INTRODUCTION

This report covers the enhancements made to the Aerospace Medical Research Laboratory (AMRL) COMBIMAN program, the efforts to standardize the AMRL Anthropometric Data Bank, and the research support provided for studies describing the strength characteristics of AF personnel.

The work documented in this report is a direct outgrowth and represents a continuation of the development and documentation of AMRL's Computerized Biomechanical MAN-model (COMBIMAN) program. The COMBIMAN program has been developed to provide the workstation engineer with an interactive graphics program to be used in the design and evaluation of aircraft cockpits. This report describes the procedures developed for the generation of the link system and enfleshment of the COMBIMAN man-model. It also documents features which enable the user to obtain visibility plots and hard copy plots of the man-model and workstation configurations.

This report also documents the continuing effort in developing and standardizing computer programs designed for the efficient analyses of anthropometric data for guiding the design of AF systems and equipment. In particular it describes the computer program developed to plot multiple survey bivariate tables, the research performed on AMRL-supplied biostereometric data, and the standardization effort dealing with the programs and the anthropometric survey data tapes of the AMRL Anthropometric Data Bank.

SECTION 2

FURTHER DEVELOPMENT OF THE COMBIMAN PROGRAM

This section documents the continued development of AMRL COMBIMAN (COMputerized BIomechanical MAN-model) program, as performed by UDRI personnel during this contract period. The three primary areas covered in this section are the enfleshment procedures established for the man-model, the plot program developed to generate hard copy plots of the man-model and workstation as displayed on the IBM 2250-3 Cathode Ray Tube, and the on-line generation of visibility plots. Another area of development which will not be documented here is the COMBIMAN User's Guide (Reference 1), written during this contract period. It reflects the operational status of the COMBIMAN programs as of 1 November 1976.

2.1 ENFLESHMENT OF THE MAN-MODEL

The man-model used in COMBIMAN is based on a 33-link skeletal system. Each of these links connects major points of rotation of the body segments. The model is constructed by the interactive graphics program of COMBIMAN in three stages. The first stage is the generation of the link system of the model. The second stage involves the definition of the enfleshment ellipsoids about the link system joints. The third stage is the connection of the elliptical projections with tangent lines.

2.1.1 Generating the Link System

Although 33 links are defined for the man-model, two of these links are positioning links, and are used to provide a common reference between the seat reference point of the model and the workspace. The links system is constructed by adding links together to form a link chain, starting with the link at the seat reference point (SRP). As each link is positioned, the link end point, or joint location, is defined in terms of a position vector,

with respect to the SRP. The major points of rotation of the body segments are shown in a side view of the model in Figure 1. Work of the Aerospace Medical Research Laboratory (AMRL) with two dimensional drawing board manikins formed the foundation for the three dimensional link system of the COMBIMAN model. AMRL data have been used in defining relationships between measurable anthropometric surface dimensions and difficult to measure internal link lengths, and in defining the range of values for transformation or Euler-type angles used to position the links.

When using the COMBIMAN interactive graphics program CBM04, the user has the ability to vary the proportions of the model to suite the needs of the application. The user may supply values as dimensions or percentiles for a variable number of anthropometric surface dimensions, or may insert the internal link lengths directly. To alter the position of the model, the user changes any of the values for the Euler-type angles available for each link. More information on the procedures for altering the dimensions of the model is given in the COMBIMAN User's Guide - (Referencel).

At the present time the equations used to establish the internal link lengths have not been validated against real life data. This is to be done in the upcoming contract period. Because they have not been validated, actual equations based on AMRL supplied data will not be presented in this report.

In assembling the individual links called L_i to establish joint locations in three dimensional space, the length and the three-dimensional Euler-type angles of a particular link are used, along with the three dimensional coordinate of the previous link, L_{i-1} , and the product of the transformation matrices which positioned L_{i-1} . The three Euler-type angles used for each link correspond to the three rotations of the coordinate axis of the system about link L_i to establish its location relative to link L_{i-1} . If all the Euler angles between adjacent links are specified, the geometric configuration of the man-model is specified. A more detailed description of the use

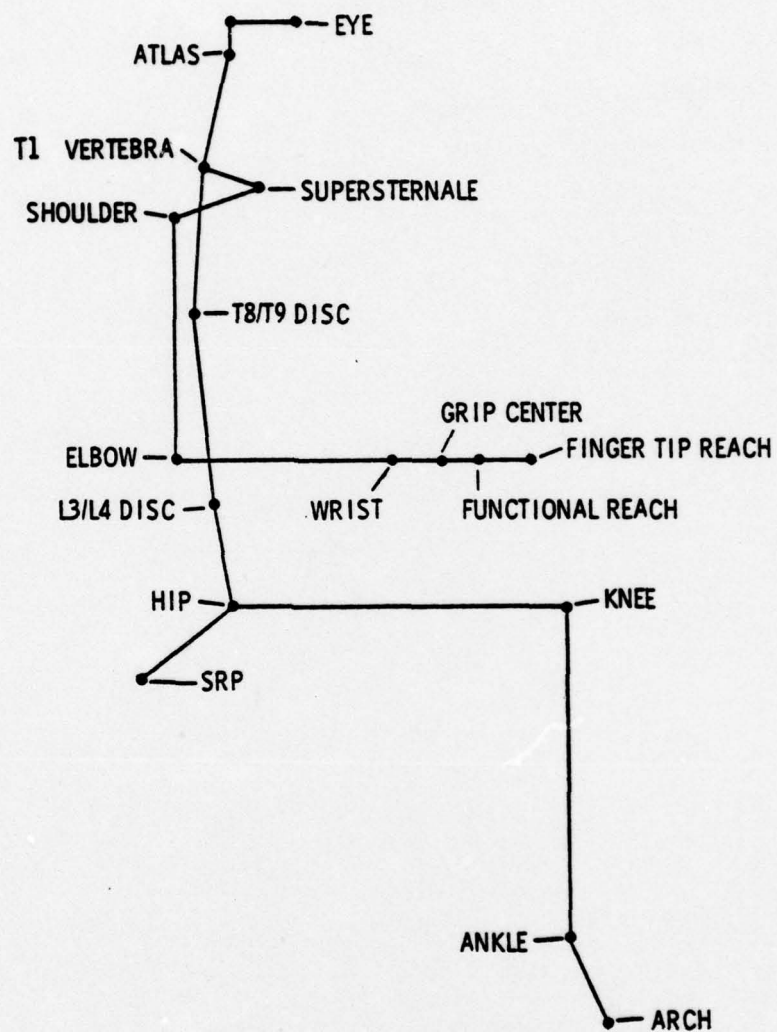


Figure 1. Side View of COMBIMAN Link System (Reference 2).

of transformation matrices and the establishment of joint locations, see Chapter 2 in Reference 3. This technique of positioning links places realistic limitations on the range of mobility of each joint and permits the repositioning of the distal link, L_i , by movement of a proximal link, say L_{i-1} .

2.1.2 Enfleshment Ellipsoids

The enfleshment, or addition of volume about the links, of the stick man-model to produce a realistic and anthropometrically correct man-model starts with the joints of the stick man-model. The joint at the distal end of each link is surrounded with an ellipsoid (three dimensional ellipse) for this purpose, as shown for a side view of the model in Figure 2. Figure 3 shows a system of coordinates for a joint at the distal end of the link L_{I_i} . This is known as the "link's system of coordinates." It is permanently attached to the end of the link, and moves with it in space. It is used to define the orientation of the next distal link which is attached to the joint.

The size and shape of an ellipsoid is defined by the dimensions of the semiaxes a , b , and c in Figure 3. These dimensions are based on body surface and mass dimensions, and derived from equations supplied by personnel of AMRL/HED. The semiaxes dimensions for each joint correspond to the height, width and breadth surface dimensions at that joint.

The position of the ellipsoid in space is determined in relation to the individual link's system of coordinates. The dimensions α , β , and γ in Figure 3 specify the distances by which the center of the ellipsoid is offset from the origin of system of coordinates in the x , y , and z directions respectively. The ellipsoid is centered at the origin of the system of coordinates, and therefore about the center of rotation, if $\alpha = \beta = \gamma = 0$.

The angular alignment of the ellipsoid is another necessary quantity to define its position. The y axes of the links' system of coordinates of the present stick-man model have been aligned with the major axis of rotation of the joint. The semiaxis b of the ellipsoid is aligned with this major

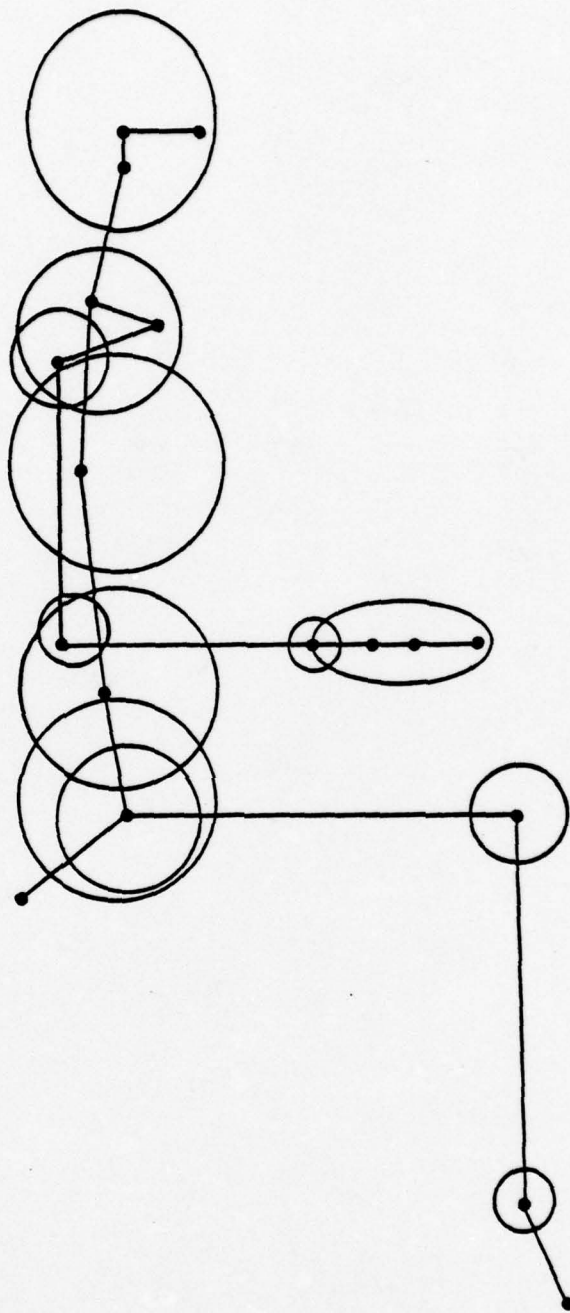


Figure 2. Side View of COMBIMAN With Enfleshment Ellipses (Reference 2).

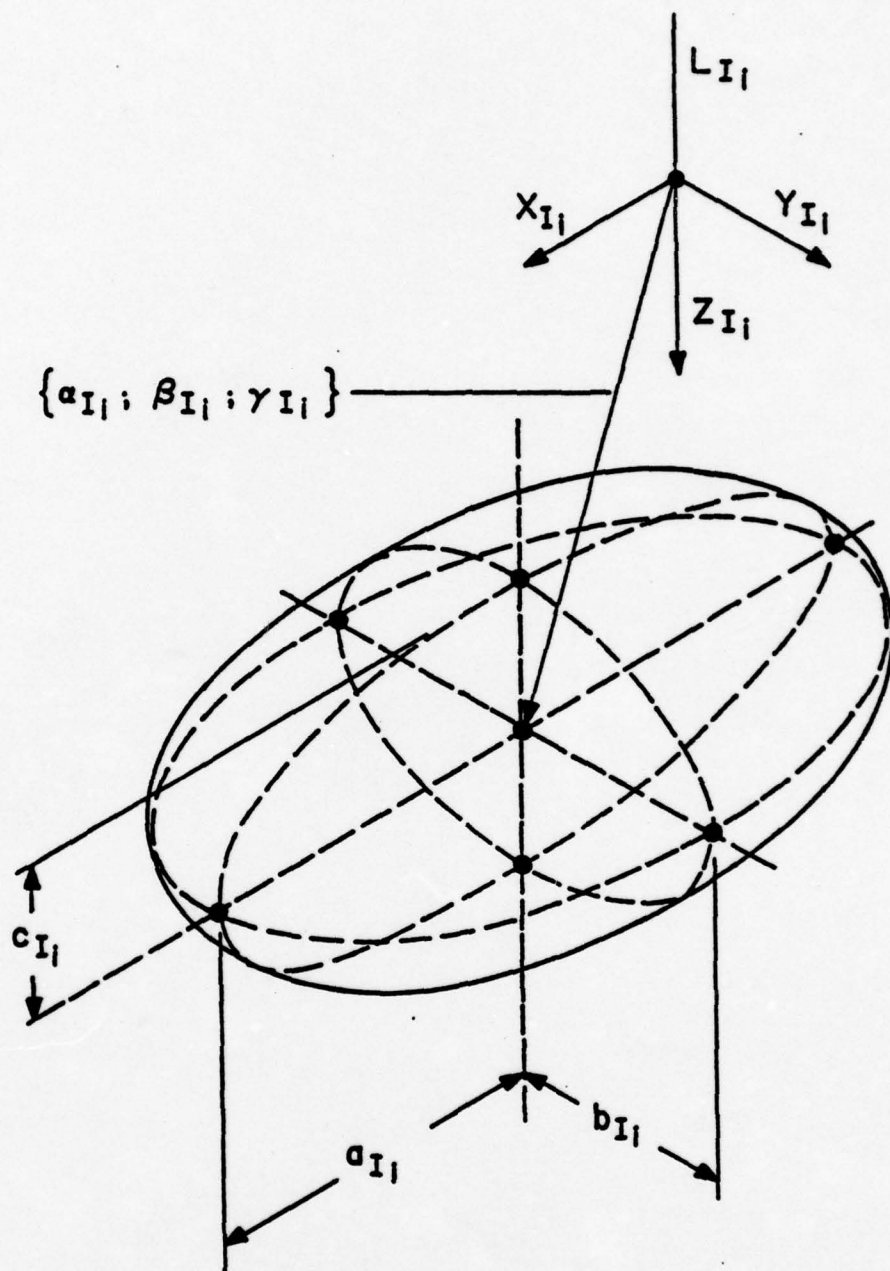


Figure 3. Ellipsoid Surrounding the Distal Joint of Link L_{I_1} .

axis of rotation. All ellipsoid axes are parallel to the axes of the link system of coordinates. This alignment produces a realistic contour of highly flexible joints at any degree of joint flexion or extension. The semi-axes a and c will have identical dimensions in most flexible joints. The cross sectional area of the ellipsoid in planes parallel to the z - x plane is thus circular. This enables the ellipsoid to function like a ball joint and to maintain anthropometrically realistic dimension in several directions.

The COMBIMAN man-model is displayed by projecting two orthogonal views on a cathode ray tube screen. The ellipsoids surrounding the joints are also projected into the screen. These projections are ellipses and are identical to the shadow of the ellipsoids produced by a source of parallel light perpendicular to the viewing screen. The man-model can be rotated and magnified or reduced within the viewing area. Any such manipulation changes the shape and/or size of the projected man-model. Any such manipulation will also change the shape and size of the shadow of a given ellipsoid on the cathode ray tube screen. The essence of the joint enfleshment stage is the definition of the projected ellipses under all conditions of body positions and viewing angles.

The projected contour of the ellipsoid onto a screen is identical to the crest (visible outer boundary) of the ellipsoid. The equations which have been developed by UDRI in conjunction with AMRL personnel are defined in detail in Section 2 of "The COMBIMAN Enfleshment Procedure and Expanded Joint Mobility Analysis", published as UDRI-TR-76-18, by the University of Dayton Research Institute in September, 1976.

The equations which are used to establish the lengths of the semi-axes a , b , and c for each joint, have not yet been validated against actual subject data. This, like the validation of the data used in stage one, is a key task to be accomplished during the next contract period.

2.1.3 Tangent Line Connectors

The last stage of the man-model generation is the connection of the elliptical contours of adjacent joints with tangent lines. This is done separately for all the contours in each viewing plane. Figure 4 shows a side view of the model with the tangent lines added. In this figure, unnecessary elliptical outlines have been eliminated. The present COMBIMAN program retains all outlines on the various views.

The equations used to establish the location of the endpoints of the tangent lines were developed by AMRL/HED personnel, in particular Dr. Joe McDaniel. The procedure used requires two sets of points which define the contours of two ellipses, each around a point of origin, with a link connecting them. One of the points of origin, and the set of points about it will be called proximal, and the other point will be called distal. From a point along the line passing thru the proximal and distal points, but beyond the proximal point, compute the slope of lines connecting this new point with each of the points on the distal ellipse. Locate the minimum and maximum slopes. From the point used in defining the maximum slope to the proximal projection, calculate the slopes to each point on the distal projection, and locate the minimum slope. From the first point used to define the first maximum slope, calculate the slope to each point on the proximal projection, and find the minimum slope. From the point used in defining this last minimum slope on the proximal projection, calculate the slopes to each point of the distal projection, and locate the maximum slope. A more detailed explanation of this procedure is shown in the flowchart in Figure 5.

The points which are located in steps 2 and 3, and 4 and 5 in Figure 5 define the endpoints of two tangent lines connecting adjacent links for one view of the model. This procedure is repeated for each combination of elliptical projections of adjacent links, for each view of the model.

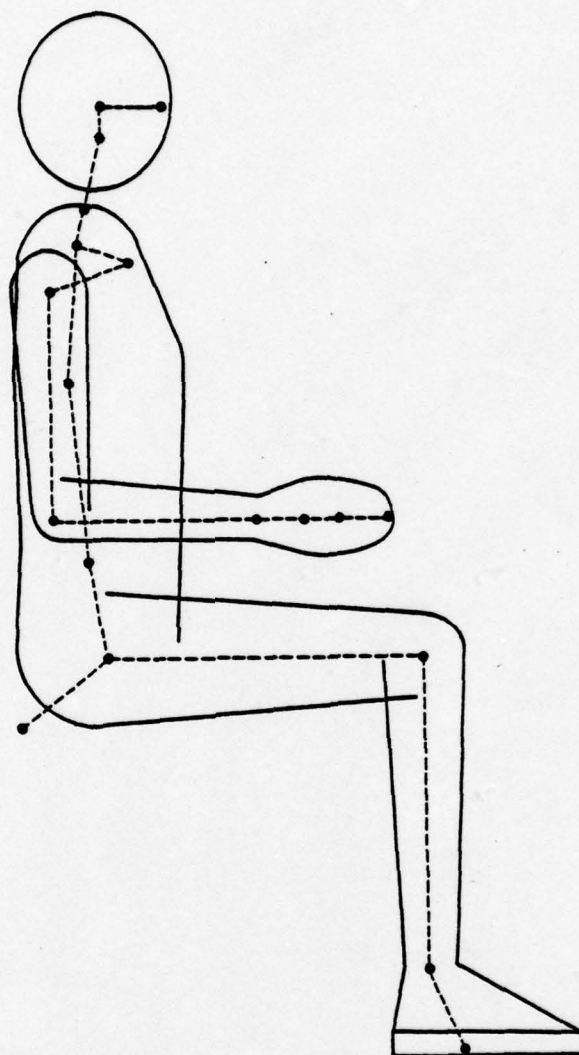


Figure 4. Side View of COMBIMAN With Tangent Lines (Reference 2).

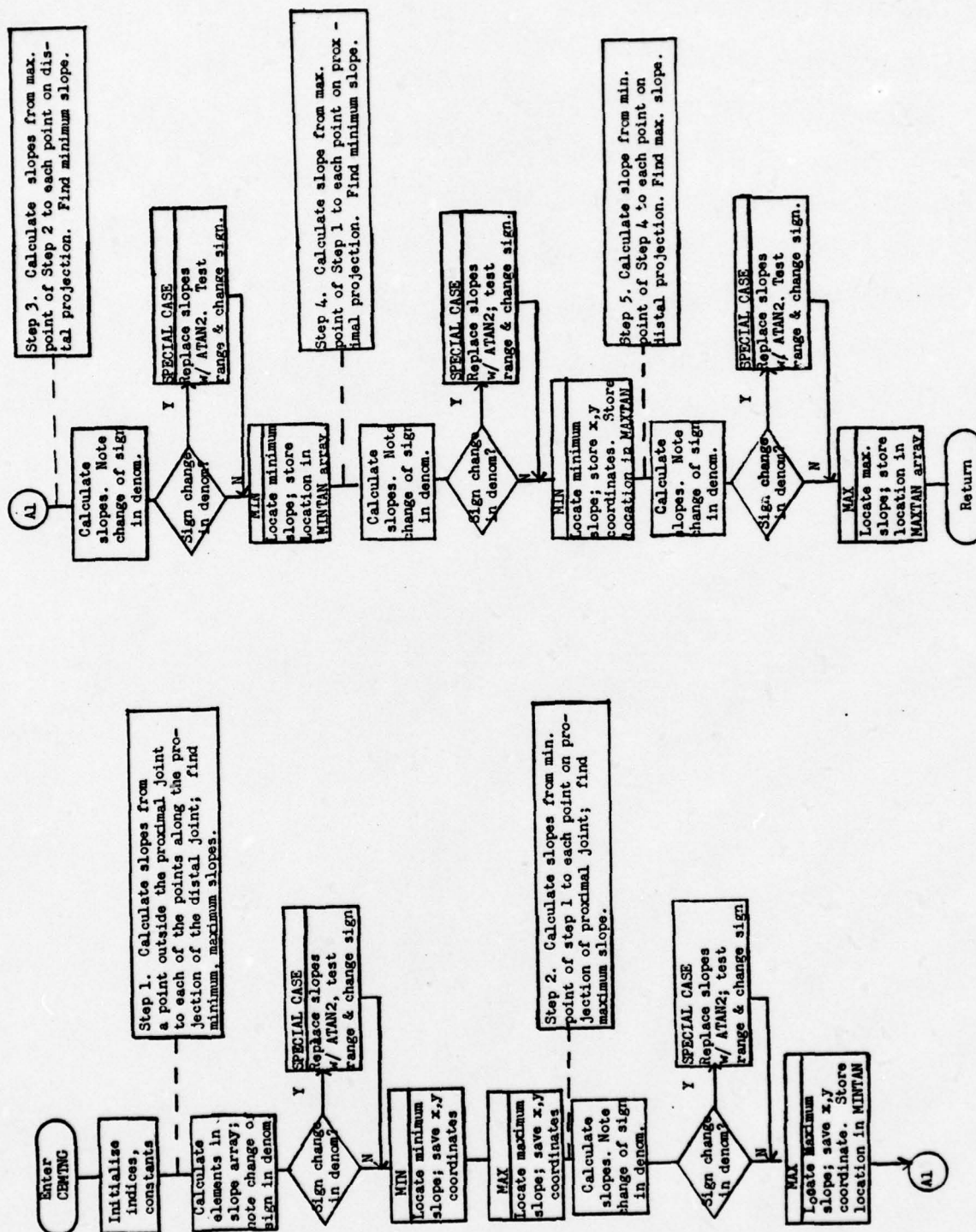


Figure 5. Flow of Tangent Line Subroutine.

Because of the nature of certain adjacent links, the enfleshment ellipses may appear to be concentric at certain viewing angles. Eventually, the tangent line subroutine will be able to detect this, and not calculate tangent line endpoints. At the present time, however, it attempts to calculate tangent lines, and often generates unusual results. An example of concentric ellipses in the side view is shown in Figure 6. The "tangent lines" connecting the MID-HIP projection and the RIGHT UPPER THIGH projection lay within the outer projection, creating unnecessary clutter on the display for the viewer.

The subroutine of the interactive graphics program CBM04, which issues the graphics orders to plot the man-model on the IBM 2250 CRT, uses the x, y, and z coordinates which define the endpoints of each link with respect to the SRP of the model. It uses the coordinates two at a time, however, to project the X-Z (side) plane, and the Y-Z (top) plane of the model (giving two orthogonal views). One view is completely generated, combining the link vertex data with the elliptical projection and tangent line coordinates for that view. The generation of and use of data for X-Y (top) plane is optional, but the user may decide to calculate this extra set of projections and tangent lines for use in hard copy - plots of the man-model/workspace configuration. The hard copy plots are discussed in the next paragraph.

2.2 PLOT COMBIMAN

In order to obtain hard-copy representations of the man-model and workstation configuration currently being displayed on the IBM 2250 Cathode Ray Tube (CRT), subroutines were developed and added to the COMBIMAN interactive graphics program CBM04 to generate two to three two dimensional plots on the HESS's on-line GOULD electrostatic plotter. The subroutines use the data arrays of three dimensional real world coordinates which are contained in computer memory and which represent the configuration of the link system of the model, the points on the elliptical projections, and the panels of the workstation. The subroutines also use data on the range of

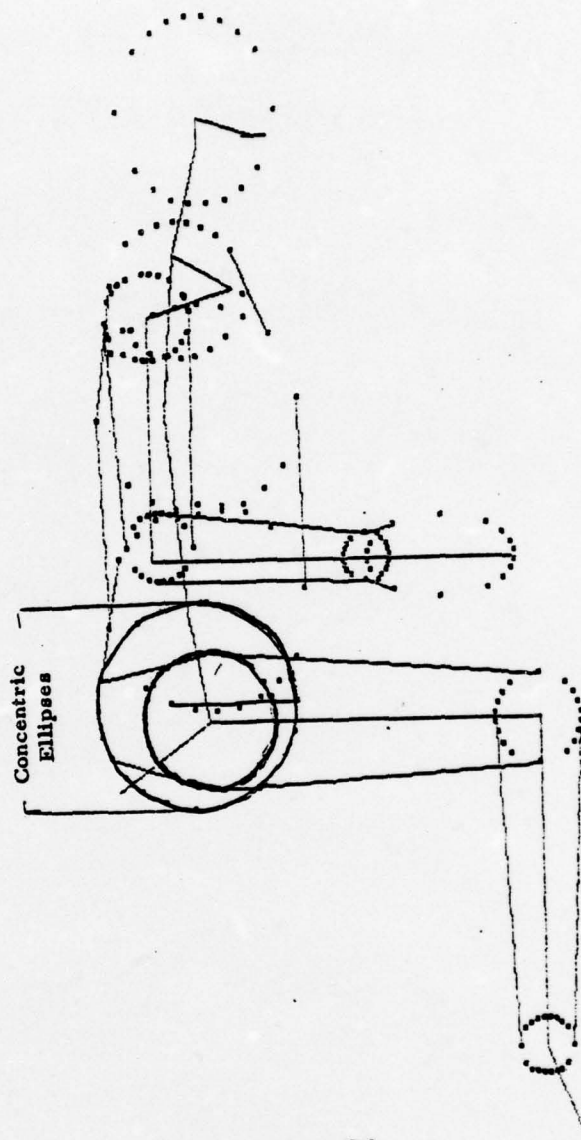


Figure 6. Side View of Model With Concentric Ellipses at Mid-Hip and Right Hip Identified.

x, y, and z-values contained in the arrays. These data were originally calculated by the subroutine which scales coordinate data to fit in the display area of the CRT and issues the graphics orders to generate the display. The range-data used include the maximum x, y, and z-coordinates found among the points, the ranges over x, y, and z-values, and the maximum of the three ranges.

2.2.1 Data Preparation

The user of the interactive graphics program has two options for specifying the size of the plots to be generated. The user can specify a scale factor from 0. to 1. or can omit any scale factor. For specific instructions on entering scale factors, see Paragraph 2.2.8 of the User's Guide for the Programs of COMBIMAN, AMRL-TR-76-117 (Reference 1). If no scale factor was supplied, the subroutine uses a factor which will scale the coordinates so as to make optimum use of a nine by nine inch plot area for each view. Once a scale factor has been established, the x-coordinates in the data arrays are scaled as follows:

$$\text{NEWX} = (\text{R-WX} - \text{XMAX} + (\text{MAXDIF} - \text{XDIF})/2.0) * \text{SCALE}$$

where:	NEWX	is the scaled x-coordinate value
	R-WX	is the unscaled x-coordinate value in the COMBIMAN base system of coordinates
	XMAX	is the maximum x-coordinate of all the coordinates in the x-coordinate data arrays
	MAXDIF	is the maximum range of coordinates in either the x, y, or z direction
	XDIF	is the difference between the minimum x-coordinate value and the maximum x-coordinate value
	SCALE	is the available scale factor

The y and z values are scaled similarly, using the following equations.

$$NEWY = (R-WY - YMAX - (MAXDIF - YDIF)/2.0) * SCALE$$

and

$$NEWZ = (R-WZ - ZMAX - (MAXDIF - ZDIF)/2.0) * SCALE$$

2.2.2 Plotting

Before the plots of the model and workstation are generated, the main subroutine prints the names of the anthropometric and regression survey used in generating the model, and the name of the workstation used, if one is being used on the plotter. From two to three plots are then generated of the two dimensional views of the model and workstation. The two views which will always be generated are of the X-Z plane and the Y-Z plane. If, prior to selecting the plot COMBIMAN function, the user selected State Switch 11, a third view of the X-Y plane will also be generated. A detailed description on setting State Switches is given in Paragraph 2.2.22 of the User's Guide (Reference 1). A general flow diagram of this main subroutine is shown in Figure 7. The actual plots are generated in a second plotter subroutine which calls the routines of the GOULD Plotter Package (see Reference 4), and plots the link system of the model, enfleshment projections, and the workstation panels for the view in question. A flow diagram of this second subroutine is shown in Figure 8. A complete plot, with three views of the model and workstation is shown in Figure 9.

2.3 GROUND VISIBILITY PLOTS

A subroutine has been added to the COMBIMAN interactive graphics program which enables the user to obtain ground visibility plots. The routine uses the eye location of the man-model in place of a camera lens, as used in AMRL-TR-69-123 (see Reference 5). The routine also provides the user with a cockpit visibility record. The boundary coordinates of objects to be plotted are obtained from engineering drawings of typical aircraft cockpits. The boundary coordinates, in the aircraft system, are read into the subroutine and first converted to the seat reference point coordinate system of the man-

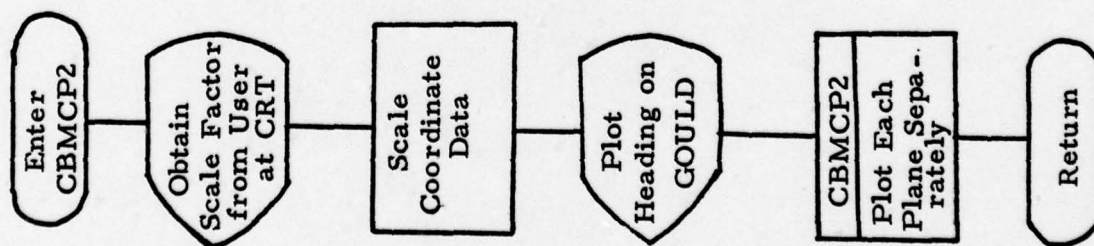


Figure 7. Flow Diagram for Subroutine CBMCP1.

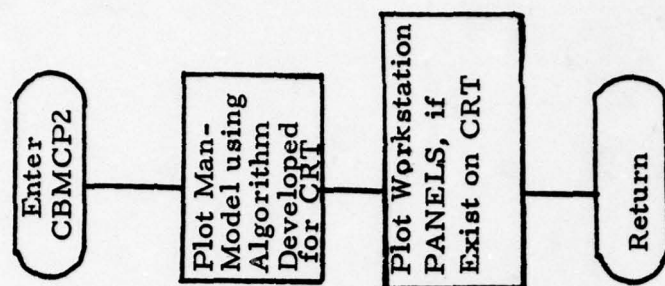


Figure 8. Flow Diagram for Subroutine CBMCP2.

REGRESS=REGRES01
SURVEY=67SURVEY
WKSP= A7E-01.

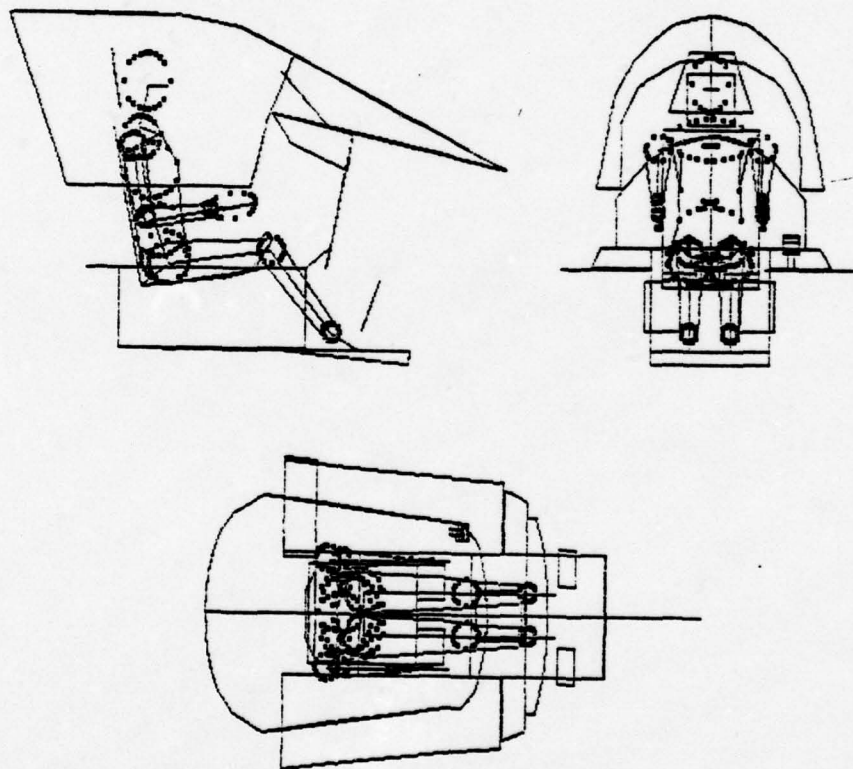


Figure 9. Sample Plot of Man-Model and Workstation from X-Z
Y-Z and X-Y Planes.

model, and then to the eye coordinate system of the model, with either the mid-eye, right eye, or left eye point of the man-model being the new origin. The eye point used by the subroutine is determined by the user. The routine then calculates the viewing angle of the model with respect to horizontal and vertical, and uses these angles to establish the cockpit visibility records.

The Visibility Plot subroutine calculates the limits of the fields of vision of the present configuration of the model and superimposes these limits over the boundary coordinates of objects of an existing workspace. It then plots them both on an on-line GOULD plotter. At the present time, the workspace which is being used is that for the A7 cockpit.

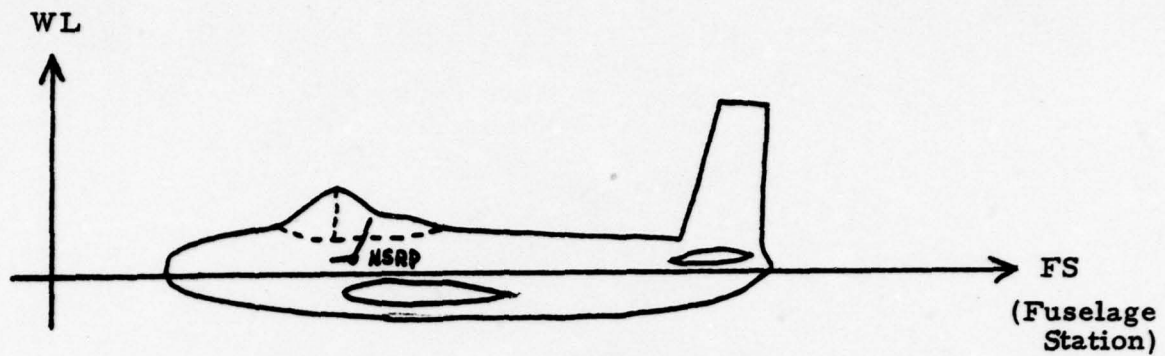
As the necessary engineering drawings for more workspaces become available, more boundary coordinates can be typed onto computer cards and added to a special disk file and be made available to the user.

2.3.1 Workspace Outline Coordinate Data Input

Data for use by the visibility plot subroutine are originally obtained from engineering drawings. The three dimensional boundary coordinates of objects to be plotted, such as aircraft canopies, windscreens, and other key outlines, are obtained in the aircraft system of coordinates. The orientation of this system is shown in Figure 10. In addition to gathering coordinate data on the key boundaries in the workspace, the location of the neutral seat reference point in the aircraft coordinate system must also be obtained. When collecting points along the boundaries, it should be noted that the greater the number of points supplied to the subroutine, the smoother the plot will be. The maximum number of points allowed for any one boundary is 200.

Once the data are obtained from the engineering drawings, they should be punched onto computer cards using the formats shown in Figure 11. The first card is punched using the format in Figure 11a. This is done once for the complete set of workspace outlines being considered. The first field on the card, NBND, contains the number of boundaries to be contained in this visibility plot. This value is an integer value, and should be right justified in the five

(Waterline)



(Buttline)

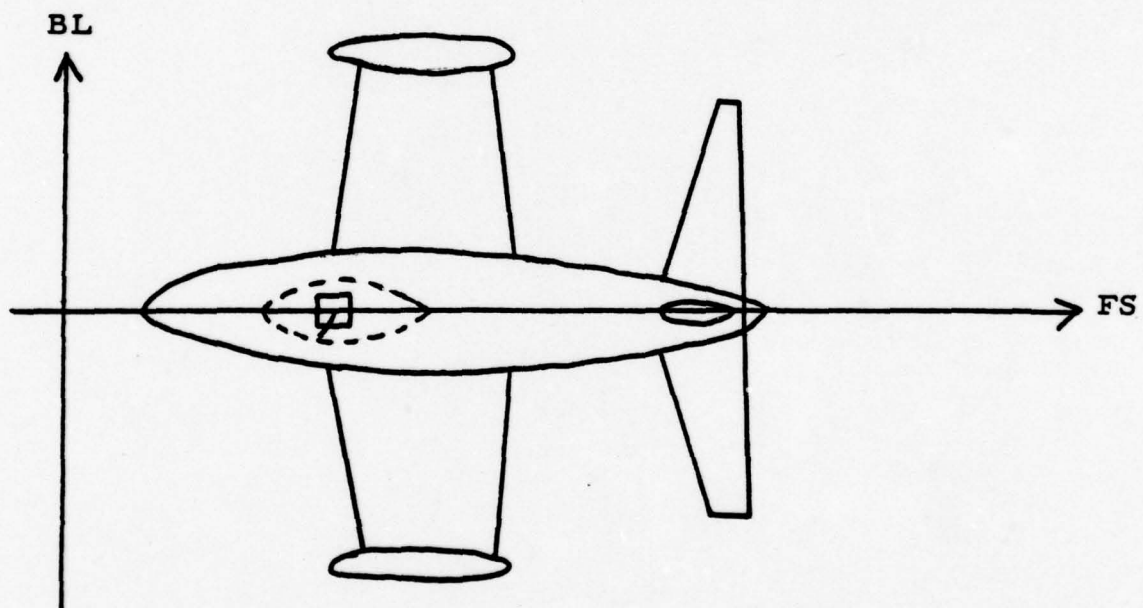


Figure 10. Orientation of Aircraft System of Coordinates.

Company

Application

by

Date _____

Job No.

Sheet No.

[illegible]

(a) Visibility Plot Control Card Format.

[illegible]

NCOORD	BOUNDARY NAME
999999	
1 2 3 4 5	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80	

XCOORD	YCOORD	ZCOORD
9999999	9999999	9999999
1 2 3 4 5	7 8 9 10 11	12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80

(b) Boundary Definition Card Format.

(c) Boundary Points Card Format.

[illegible][illegible]

Figure 11. Input Formats for Visibility Plot Subroutine.

digit field. The next three fields (XAC, YAC, ZAC) define the location of the neutral seat reference point in the aircraft system of coordinates. These coordinates are real values and assume a format of F5.3 if no decimal point is supplied by the user. The last three fields of this card define the location of the seat reference point of the COMBIMAN model with respect to the neutral seat reference point of the aircraft. At the present time these values should be zero or left blank. In the near future they will be obtained from the interactive graphics program CBM04 to reflect variations in the location of the seat with respect to the original neutral seat reference point.

The second and third formats shown in Figure 11 are used for each boundary. The format in Figure 11b contains the number of coordinate sets, NCOORD, which will be used to define this boundary. It is an integer value, and should be right justified in the five digit field. This card also contains an alphanumeric name for the boundary in field BOUNDARY NAME. The name may not be more than 24 characters long. The format shown in Figure 11c is used to define the three coordinates for each point along the boundary. The three coordinates are to be supplied in the aircraft system, and are typed using a F6.2 format. Sample coordinate data for the A7 cockpit is shown in Figure 12. The workspace is defined in terms of three configurations, the Front Bottom Windscreen, the Front Top Windscreen, and the Cockpit Canopy Clearline.

Once all the data have been punched onto computer cards, they are written onto a disk file for use by the interactive graphics program CBM04. The Job Control Cards (JCL) for accomplishing this are shown in Figure 13. The first outlined area in Figure 13 lists the JCL needed to call an IBM utility "IEHPROGM" which scratches any dataset containing workspace boundary data which may exist on disk. The second outline area shows the JCL needed to call the IBM utility "IEBGENER" and create a new dataset called "SME. VISDATA" which will contain the boundary coordinate data available on cards. The third outlined area lists the JCL used to call the IBM utility "IEBGENER"

<pre> //VISFILE JOB (UDR807,K0),EVANS,MSGLEVEL=1 //SCRATCH EXEC PGM=IEHPRQGM //SYSPRINT DD DUMMY //PUBLIC DD VOL=SER=PUBLIC,UNIT=3330,DISP=OLD //SYSIN DD * SCRATCH DSNAME=SME.VISDATA,VOL=3330=PUBLIC /* //RECRT EXEC PGM=IEBGENER //SYSUT2 DD DSN=SME.VISDATA,DISP=(NEW,CATLG),UNIT=SYSDA, // VOL=SER=PUBLIC,SPACE=(1600,(10,5),RLSE), // DCB=(LRECL=80,RECFM=FB,BLKSIZE=1600,DSORG=PS) //SYSPRINT DD SYSOUT=A,DCB=BLKSIZE=121 //SYSIN DD DUMMY //SYSUT1 DD * </pre>	1
<p style="text-align: center;">BOUNDARY OUTLINE CARDS GO HERE</p>	2
<pre> /* //PRINT EXEC PGM=IEBGENER //SYSUT1 DD DSN=SME.VISDATA,DISP=OLD //SYSPRINT DD SYSOUT=A,DCB=BLKSIZE=121 //SYSUT2 DD SYSOUT=A,DCB=BLKSIZE=81 //SYSIN DD DUMMY /* // </pre>	3

Figure 13. Job Control Cards Needed to Establish Data Set on Disk Containing Boundary Outlines for Visibility Plots.

again, but this time it prints the contents of the dataset "SME. VISDATA" for verification purposes. A detailed description of each of the IBM utilities used can be found in Reference 6.

Although the boundaries are described separately on computer cards, the individual subsections are automatically recombined before plotting the total visibility plot.

2.3.2 Generating the Vision Angles

The subroutine to generate the visibility plot is activated when the user of the interactive graphics program CBM04 presses the Visibility Plot Function Key (see Reference 1). This subroutine then reads the disk file which has been loaded with workspace boundary coordinates, and stores the available data for the necessary calculations in arrays in memory. If, for some reason, the disk file does not contain any workspace coordinate data, the message "NO DATA AVAILABLE FOR VISIBILITY PLOT ON UNIT 9" will be displayed in the information area of the screen. The routine is ended and the user is asked to depress another function key.

Once the function key has been depressed and the boundaries read in, the prompting area will display the message "ENTER EYE LOCATION (LINK)". The user must decide on the eye point to be used as a reference for the plots. Possible values are either 8 for Mid-Eye point, 9 for Right Eye point or 10 for the Left Eye point. These values should be typed in, right justified in the eight digit field. Once a valid link number has been specified, the message "PLOTING" is displayed on the CRT screen.

The routine uses the coordinates which define the endpoint of the Mid-Head link (link 7) and the coordinates of the Mid-Eye point to calculate the angles of sight from horizontal and from vertical. Facing forward and looking straight ahead would be angle of 0° from both horizontal and vertical.

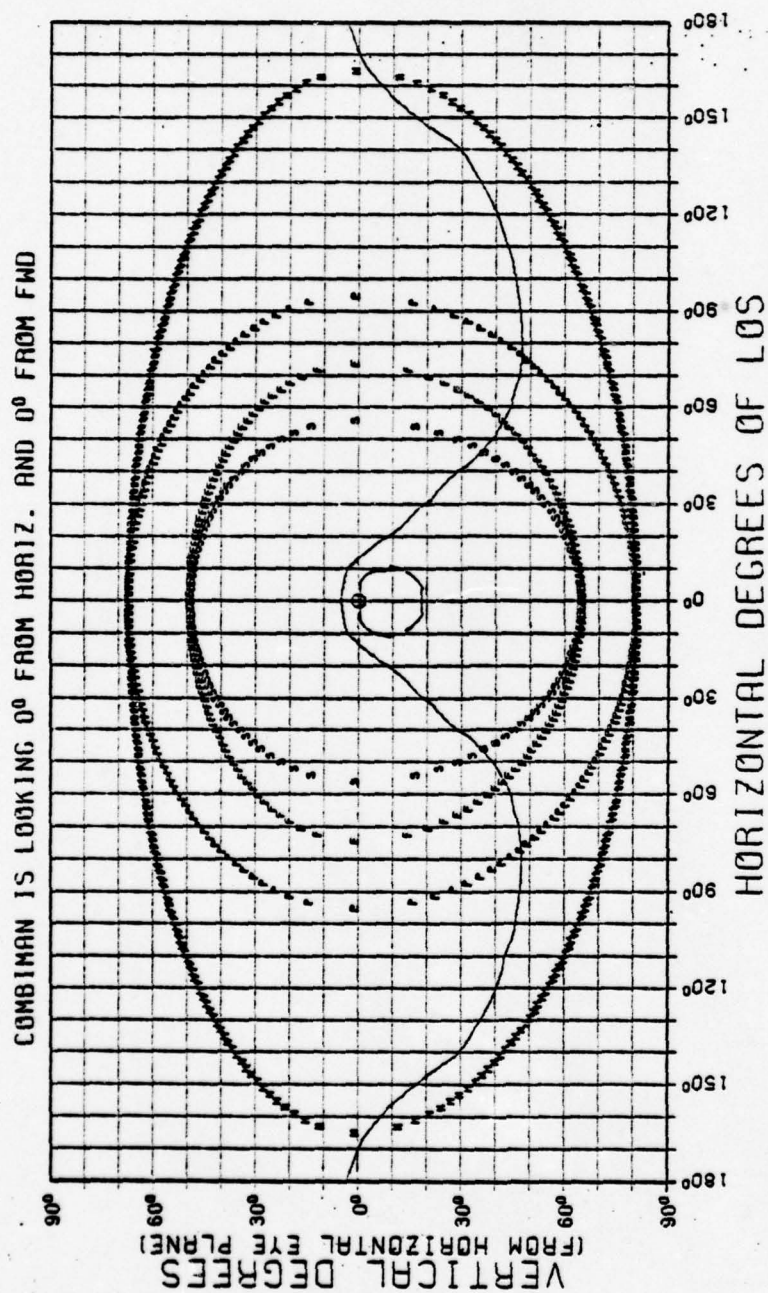


Figure 14. Sample Visibility Plot - Straight Ahead View.

Once the three dimensional coordinates of the boundary have been translated to the eye coordinate system of the model, the subroutine processes the points by iterating over the angular range of the points to determine the intersection of integer angles of horizontal line of sight with the line segment formed by two consecutive points on the workspace boundary. The angular range of points is calculated by the subroutine, and is based on the minimum and maximum horizontal angle of intersection with the workspace boundary being evaluated. The equations which are used to establish the angles of intersection and the coordinates of the boundary at these points were provided by Dr. McDaniel of AMRL.

2.3.3 The Visibility Plot And Printed Output

Figure 14 shows a sample visibility plot with the A7 outline. For this example, the man-model was positioned in a seated erect posture, looking straight ahead. The vision limits were generated with respect to the angle of sight of the Mid-Eye point (link 8).

The four ellipses on the plot define the limits of various visual fields. The inner most field, plotted with the letter S, defines the field of stereo vision, with both eyes in their normal position. The next field, plotted with the letter F, defines the right and left fixation limits of vision. The third field is plotted with the letter P and defines the limits of peripheral vision associated with the facing forward with respect to the head. The outermost field, plotted with the letter M, defines the maximum peripheral vision limits for the left and right eye. The symbol \odot defines the normal line-of-sight of the model.

The contour of the workspace boundaries are plotted with respect to the line-of-sight of the man model. As the model's head is shifted from the forward position the workspace boundaries are shifted in the opposite direction. An angle other than zero degrees from the horizontal eye plane of the model causes the boundaries to be raised or lowered based on a positive or negative angle from horizontal. The label indicating degrees on the vertical axis is

shifted in increments of multiples of ten degrees. This increment is calculated by dividing the angle from horizontal by 10., truncating this quotient to the nearest whole number, and then multiplying this value by 10. The boundaries and the visual limits are shifted slightly, so that value obtained with respect to the vertical axis is always labeled with angles which are multiples of 10. A sample visibility plot which was generated using visual angles of -15° from horizontal and 30° from forward is shown in Figure 15.

In addition to generating a hard copy plot on the GOULD unit, the subroutine also calculates and sends to the printer the three dimensional coordinates of each of the workspace boundaries in five degree angle increments from -180° from horizontal line of sight to $+180^\circ$. The coordinates are given in the aircraft system of coordinates. The listing also gives the coordinate of the eye location in the aircraft system. Figure 16 shows the coordinate data for the plot in Figure 14.

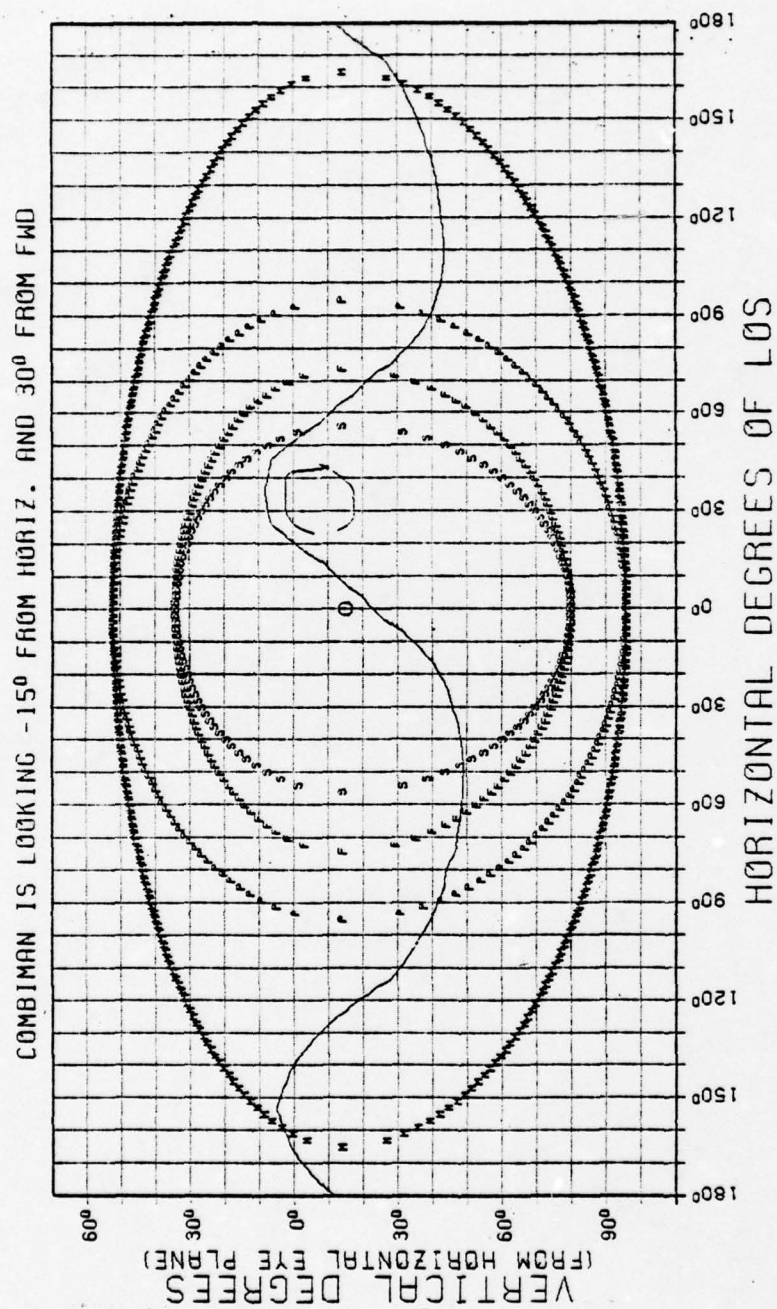


Figure 15. Sample Visibility Plot - Off Angle View.

CBNO4 --- COMBINAN PROGRAM, VERSION 4

VISIBILITY PLOT DATA FOR COCKPIT CANOPY CLEARLINE
EYE LOCATION IN AIRCRAFT SYSTEM (262.2%, 0.0, 133.58)

HORIZ. ANGLE	AIRCRAFT FS	AIRCRAFT COORDINATES BL	HORIZ. ANGLE	AIRCRAFT FS	AIRCRAFT COORDINATES BL	HORIZ. ANGLE	AIRCRAFT FS	AIRCRAFT COORDINATES BL	HORIZ. ANGLE	AIRCRAFT FS	AIRCRAFT COORDINATES BL
-180	294.470	-0.000	-60	253.086	15.891	60	253.083	-15.896	60	253.083	-15.896
-175	294.004	2.777	-55	251.547	14.729	65	254.429	-16.795	65	254.429	-16.795
-170	293.688	5.541	-50	250.899	13.543	70	256.045	-17.078	70	256.045	-17.078
-165	293.224	8.297	-45	249.938	12.323	75	257.649	-17.209	75	257.649	-17.209
-160	292.483	11.000	-40	249.109	11.036	80	259.206	-17.323	80	259.206	-17.323
-155	291.646	13.703	-35	248.522	9.620	85	260.729	-17.510	85	260.729	-17.510
-150	290.483	16.294	-30	247.982	8.244	90	262.261	-17.679	90	262.261	-17.679
-145	289.109	18.799	-25	247.567	6.852	95	263.819	-17.816	95	263.819	-17.816
-140	285.261	19.300	-20	247.212	5.477	100	265.420	-17.920	100	265.420	-17.920
-135	281.341	19.080	-15	246.559	4.100	105	267.083	-17.998	105	267.083	-17.998
-130	278.104	18.882	-10	246.775	2.731	110	268.890	-18.214	110	268.890	-18.214
-125	275.300	18.622	-5	246.692	1.362	115	270.832	-18.381	115	270.832	-18.381
-120	272.925	18.472	0	277.911	0.0	120	272.925	-18.472	120	272.925	-18.472
-115	270.832	18.381	5	246.692	-1.362	125	275.300	-18.622	125	275.300	-18.622
-110	269.097	18.783	10	246.775	-2.731	130	278.104	-18.882	130	278.104	-18.882
-105	267.083	17.998	15	246.959	-4.100	135	281.341	-19.080	135	281.341	-19.080
-100	265.419	17.913	20	247.212	-5.477	140	285.261	-19.300	140	285.261	-19.300
-95	263.817	17.787	25	247.567	-6.852	145	289.109	-19.541	145	289.109	-19.541
-90	262.261	17.647	30	247.982	-8.244	150	290.483	-19.799	150	290.483	-19.799
-85	260.729	17.510	35	248.522	-9.620	155	291.646	-19.920	155	291.646	-19.920
-80	259.206	17.323	40	249.109	-11.036	160	292.483	-20.000	160	292.483	-20.000
-75	257.658	17.178	45	249.938	-12.323	165	293.224	-20.297	165	293.224	-20.297
-70	256.050	17.063	50	250.899	-13.540	170	293.688	-20.541	170	293.688	-20.541
-65	254.429	16.795	55	251.547	-14.729	175	293.986	-20.776	175	293.986	-20.776

Figure 16. Sample Visibility Plot Printed Output for Cockpit Clearline Boundary in Figure 14.

SECTION 3

STRENGTH CAPABILITIES OF SEATED OPERATORS

The University of Dayton Research Institute supported a study to determine the capabilities of human subjects to exert forces on a triaxial force handle located within the subjects' reach. This study is being conducted by Dr. J. W. McDaniel of AMRL/HED. UDRI personnel performed modification, calibration, and maintenance of the HERCULES (Human Engineering Research to Cull Efficient Strength) apparatus located in AMRL/HED. UDRI personnel were also responsible for the collection of strength data from human subjects and the preliminary data analysis.

3.1 HERCULES LAB

The HERCULES apparatus and associated equipment has been made completely operational after a period of inactivity. Using a triaxial strain gauge transducer handle, this system can measure and record forces exerted by seated human subjects with 2% accuracy on forces up to 300 pounds in any direction. The handle was positioned in 76 locations relative to the SRP (Seat Reference Point) of the seated subject.

The equipment used for the data collection is shown in Figure 17 and consists of the triaxial force handle, a Honeywell Accudata 113 bridge amplifier system, a Honeywell 5600B 7-channel FM tape recorder, a Brush Mark 200 strip chart recorder, an audio amplifier and power supply, and a remote control unit.

3.1.1 Contractor-Built Equipment

3.1.1.1 Remote Control Unit

To simplify the experimenter's task, a remote control unit (shown in Figure 18) was designed and built to contain an exertion timer, dial encoder, strip chart ON/OFF switch, data switch, and tape

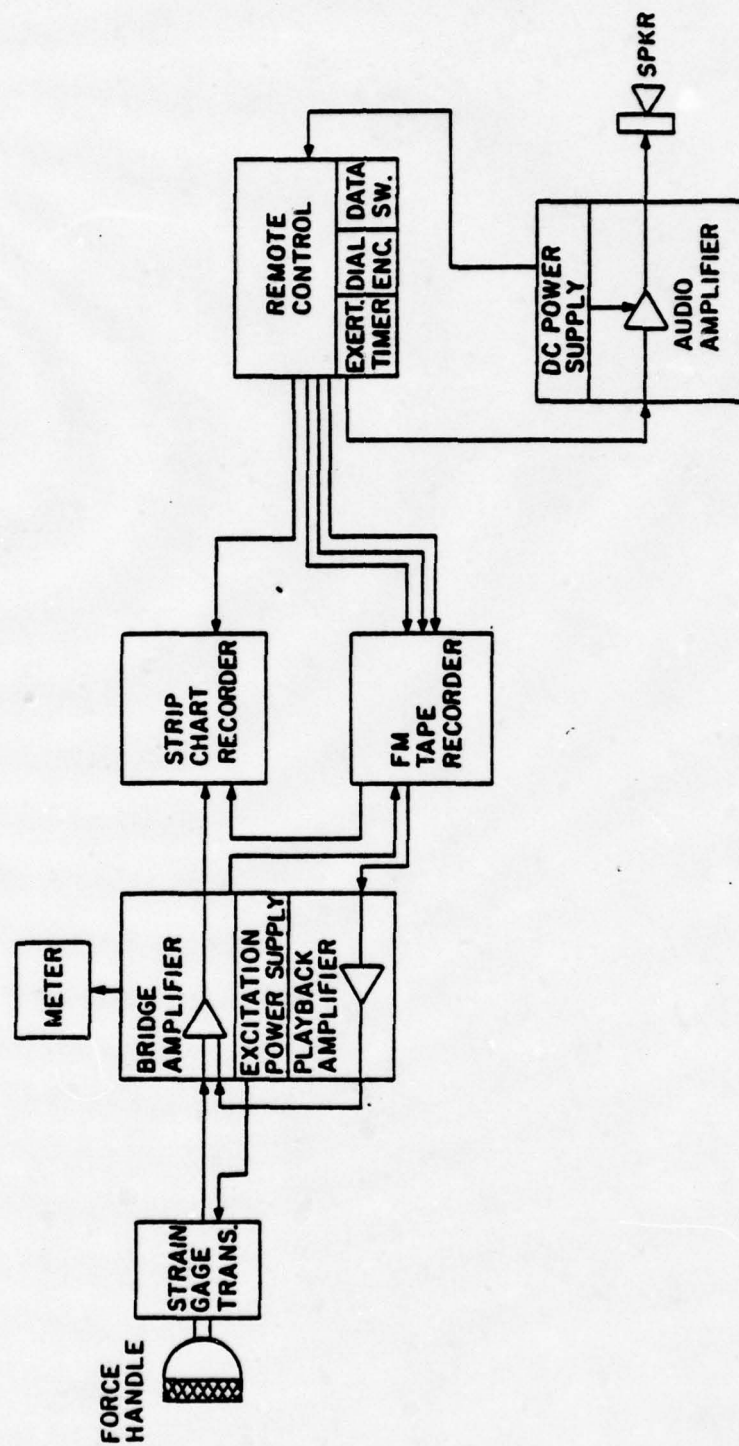


Figure 17. HERCULES System Component Diagram.

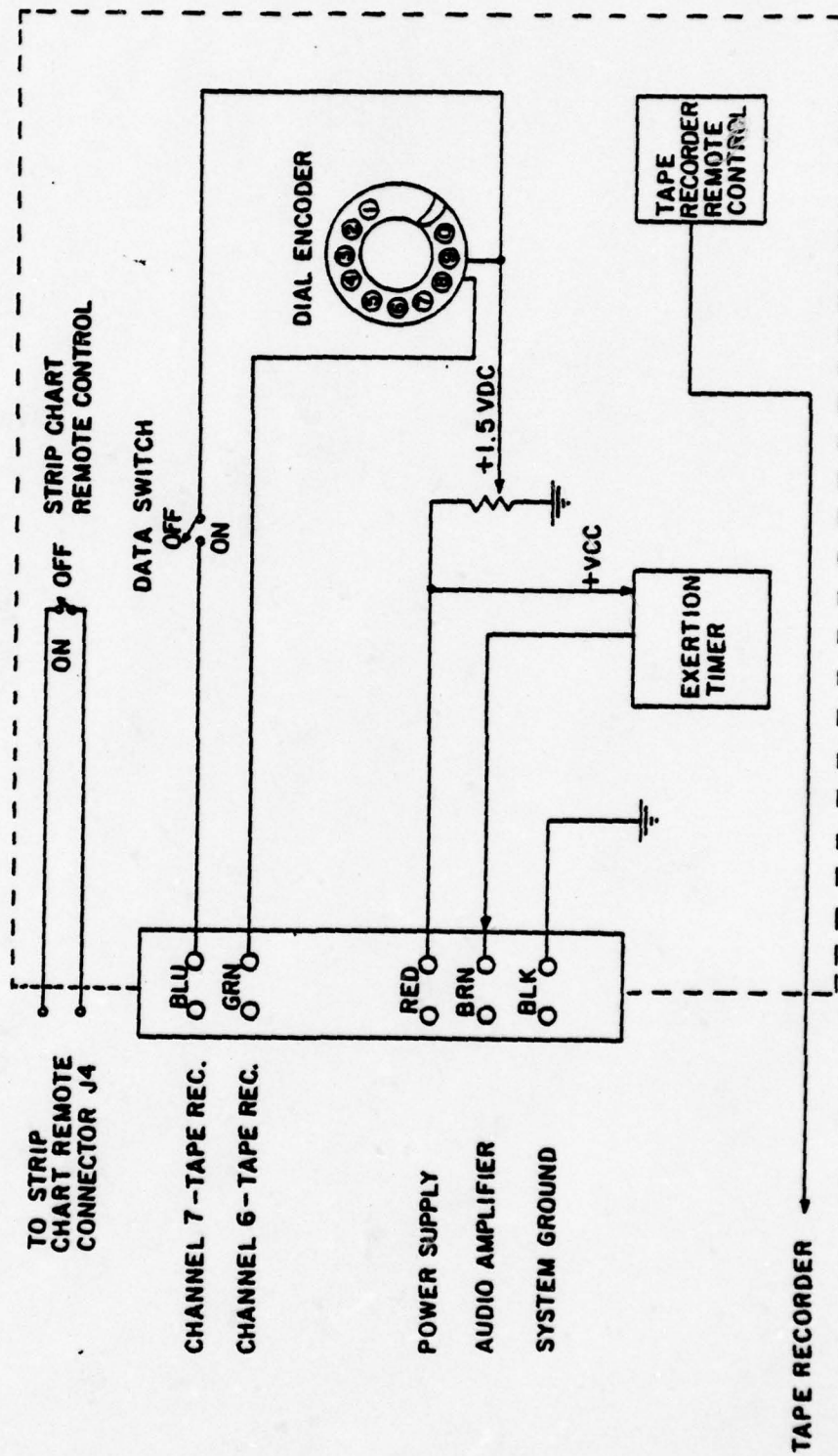


Figure 18. HERCULES System Remote Control Unit.

recorder remote control. These functions were connected to the system with a ten-foot cable. The controls on the panel were arranged according to order and frequency of use. This arrangement places all frequently used functions at the experimenter's fingertips.

To provide an edit function, a data switch was installed on the remote control unit and was used to indicate valid (ON) or invalid (OFF) data on one channel of the tape recorder.

3.1.1.2 Timer Controlled Tone Generator

An electronic timer was designed and constructed to provide an auditory tone to cue the subject as to when to terminate the exertion. The timer consisted of three ECG-955 ICs (integrated circuits) performing three basic functions within the timer. The circuit diagram is shown in Figure 19.

IC1 was triggered by a pushbutton at the beginning of a force exertion and performed the main timing function of controlling the delay interval. This interval was adjustable from zero to two minutes but was normally set to five seconds. Triggered by IC1, IC2 controlled the duration of the auditory tone and was also variable from zero to 2 minutes in length, but was normally set to a $\frac{1}{2}$ second burst. IC3 was used as an audio oscillator and was turned on and off by IC2. The output of IC3 was connected to the input of the audio amplifier as shown in Figure 20.

3.1.1.3 Audio Amplifier

The audio amplifier was on LM380 IC capable of one watt audio output and was normally set well below this level. The audio output was coupled to a common speaker. The speaker was attached to the HERCULES handle mainframe assembly near the subject.

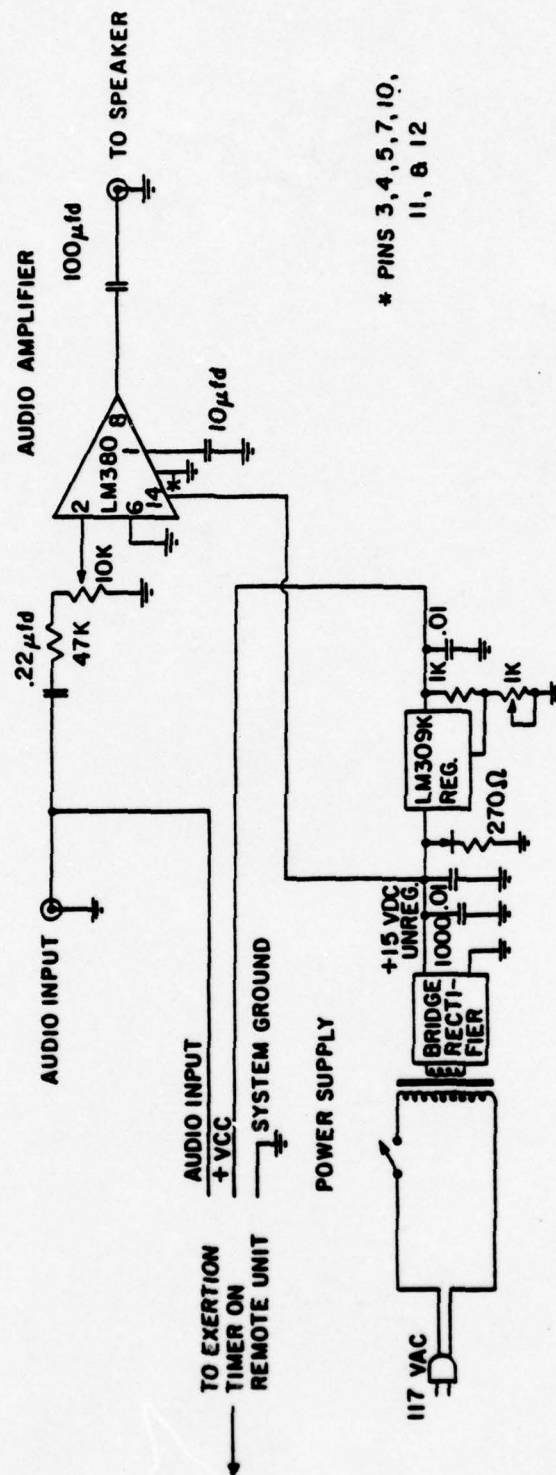


Figure 20. Diagram of the Power Supply and Audio Amplifier.

3.1.1.4 Power Supply

A power supply was built for the timer, audio amplifier, data switch, and dial encoder and is shown in Figure 20. Using an LM309K voltage regulator IC, the supply is adjustable from five to fifteen volts DC at up to 1 amp output current with internal overload protection.

3.1.2 Modifications to the Existing Equipment

3.1.2.1 Reference Resistors

The accuracy of the system has been improved through various modifications. Calibration efficiency required high-stability reference potentiometers as shown in Figure 21, to be installed and calibrated to simulate known forces in six directions. A weight stand was built to facilitate applying known forces on the handle. Its pulley system allowed a 100-pound force to be exerted on the handle in six orthogonal directions. A digital voltmeter was used to calibrate the reference potentiometers against the 100-pound weights.

3.1.2.2 Noise Level Reduction

The system originally had a high noise level due to several unshielded connections. When these were corrected, the noise was reduced significantly.

3.1.2.3 Dial Encoder

A telephone-type dial encoder was used to generate pulses to identify calibrations, subjects, and handle positions during data collection. This was installed on the remote control unit.

3.1.2.4 Tape Recorder Remote Control

This unit was installed on the remote control unit. However, there were no further modifications to it.

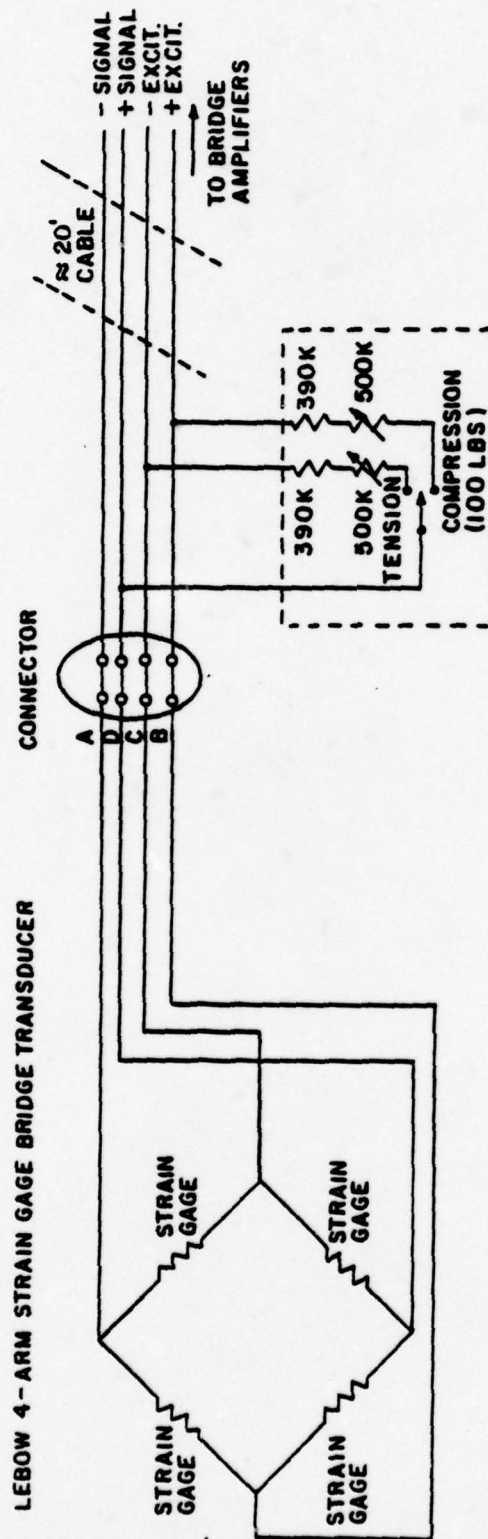


Figure 21. Diagram Representing a Single Channel of a 3-Channel HERCULES Bridge Transducer System.

3.1.2.5 Remote Strip Chart ON/OFF Switch

A toggle switch was installed on the remote control unit to provide for remotely activating the strip chart paper drive mechanism.

3.2 PROCEDURES

Data collection procedures required modifications for two reasons: the equipment modifications, and analog data processing constraints. Because of constraints of equipment capabilities of the ASD Computer Center Hybrid Simulation Division, data collection procedures were modified to facilitate the conversion of analog data.

Through the process of identifying sources of errors in the data analysis system, several procedural improvements to the analog-to-digital conversion process were recommended. Additionally, a computer program was prepared to provide a means of organizing the data collection procedure and to provide an automated check of the digital data.

3.2.1 Computer-Generated Data Collection Format

A program named RANDM has been developed for the HERCULES experiment to print an experimental data collection sequence which contains information the experimenter needs to position the force handle, select a direction of exertion, and select a subject to perform that exertion. The programmer uses the IBM System Subroutine RANDU to generate the random numbers which, in turn, are used to generate the sequence of steps to be followed in the procedure. A detailed description of the subroutine RANDU can be found in the IBM Scientific Subroutine Manual (Reference 7). All random numbers generated by RANDU are 15 digit decimal numbers between 0. and 1.

3.2.1.1 Method

In order to assure a unique set of random numbers throughout each execution of the program RANDM a new 15 digit seed number is supplied to the random number generator the first time it is called by

RANDM. A random handle position number is found by multiplying the first random number obtained from RANDU by a number which is one greater than the number of positions possible, and truncating the result to an integer value. All exertion directions are then randomized for each subject within each position using the same randomization process. If the number of simultaneous subjects is n , subject i will start as the first subject of the first position, and subject $i+1$ will start as the first subject of the next position. This sequence is continued until the n^{th} subject is reached. At this point the same sequence is repeated until all handle positions have been used. The last exertion in a sequence for a given handle position is a repetition of the first exertion direction/subject combination. For this repeated exertion, a constant (100) is added to the subject number to set it apart from the other subject numbers. This repetition is performed to provide a verification of the subject's performance reliability (see Figure 22). At the end of the program, the seed number to be used when the program is run again is printed out. This is done to make sure all numbers are randomized properly (see Figure 23). A flow-chart of program RANDM is shown in Figure 24.

3.2.1.2 Program Input Data

The first data card read by the program RANDM gives information on the number of exertion directions (nexr), handle positions (npos) and simultaneous subjects (nsub) which are to follow. Any number up to 9 exertion directions, 99 handle positions, and 5 simultaneous subjects are possible. These numbers are right justified (see Figure 25a).

The following group of nexr cards will be the exertion directions. Each card contains one exertion direction number (iexr) and its 8 character name (exertion-direction name). The exertion direction number is an integer and is right justified in the field (see Figure 25b).

The second group of npos cards read will each have one handle position number (ipos) and the three dimensional coordinates of that handle position (lat dim, fwd dim, vert dim), as shown in Figure 25c.

POSITION 4 LATERAL= -20 FORWARD= 30 VERTICAL= 30

	SUBJECT NO.	NAME	EXERTION	DIRECTION
1	7301	PAT	404	DOWN
2	7302	TOM	204	RIGHT
3	7301	PAT	504	FORWARD
4	7302	TOM	304	UP
5	7301	PAT	104	LEFT
6	7302	TOM	504	FORWARD
7	7301	PAT	304	UP
8	7302	TOM	604	BACKWARD
9	7301	PAT	204	RIGHT
10	7302	TOM	104	LEFT
11	7301	PAT	404	BACKWARD
12	7302	TOM	404	DOWN
13	7401	PAT	404	DOWN

Figure 22. Sample Data Collection Sequence, with Subject 1 Repeated.

POSITION 7 LATERAL= -20 FORWARD= 30 VERTICAL= 20

	SUBJECT NO.	NAME	EXERTION	DIRECTION
144	7302	TOM	507	FCREWARD
145	7301	PAT	607	BACKWARD
146	7302	TOM	207	RIGHT
147	7301	PAT	507	FCREWARD
148	7302	TOM	607	BACKWARD
149	7301	PAT	207	RIGHT
150	7302	TOM	307	LP
151	7301	PAT	107	LEFT
152	7302	TOM	107	LEFT
153	7301	PAT	407	CCWN
154	7302	TOM	407	CCWN
155	7301	PAT	307	LP
156	7402	TOM	507	FCREWARD

NEW SEED TO BE USED = 727020975.

Figure 23. Sample Data Collection Sequence, with New Seed Number Printed.

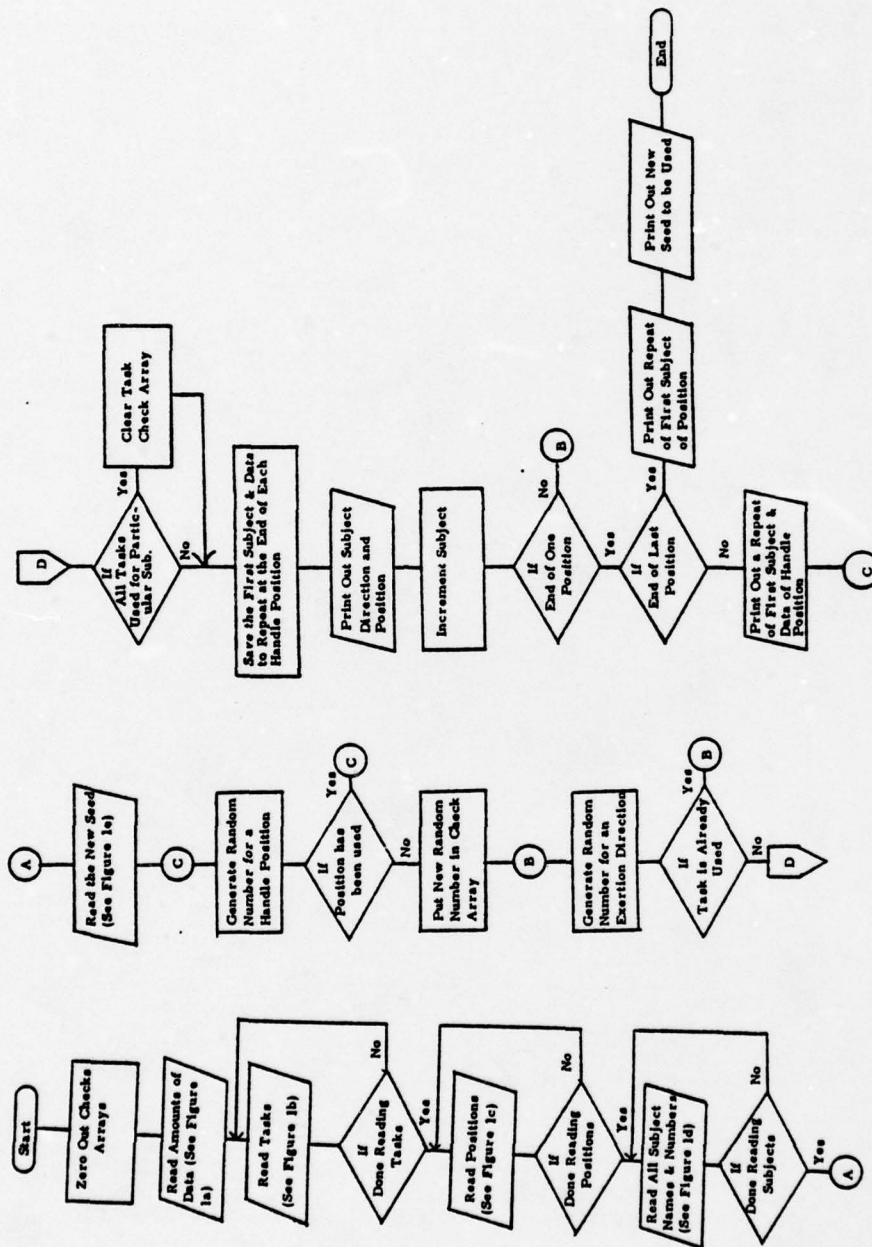


Figure 24. Flow Diagram for Program RANDM.

The third group of nsub cards read will each contain one subject number (isub) and the subject's first name (subject name). The subject number is an integer value and should be right justified (see Figure 25 d).

The last card read should be the initial seed number for the program. The seed is right justified and must have a decimal point at the right-most position (see Figure 25e).

3.2.1.3 Program Output

The first output format generated is a repeat of the input data. This provides a means of verifying the input data (see Figure 26).

The second output format contains random position number, its three-dimensional coordinates, and its associated experimental data collection sequence. This consists of all exertion directions, randomized for each subject. This format will be used for all handle positions. No handle positions are repeated, and for each position no exertion directions are repeated for any one subject.

In addition to printing the output on paper this program will also punch the output data on cards for use in verifying the experimentally gathered digital data.

INPUT

0 12 2
1 LEFT
2 RIGHT
3 UP
4 DOWN
5 FORWARD
6 BACKWARD
1-20 20 40
2-20 10 40
3-20 0 40
4-20 30 30
5-20 20 30
6-20 10 30
7-20 30 20
8-20 20 20
9-20 10 20
10-20 30 10
11-20 20 10
12-20 10 10
7301 PAT
7302 TCM
1397643.

Figure 26. Repeat of Input to Program RANDM.

SECTION 4

MULTIPLE BIVARIATE PLOTTING PROGRAM (BIVPLOT)

A considerable effort was made during this contract period to develop a plotting program (BIVPLOT) to plot the frequencies of two anthropometric variables which the user has selected from two surveys. The frequency data from the two surveys are plotted within the same table. Built into BIVPLOT is the capability of producing single survey tables as well. Both of these can be used with data in either English or metric units. Only the general layout and statistical computations could be used from the existing AMRL bivariate program which was made to produce single surveys on a computer line printer. An example of the output of this program is shown in Figure 27. While attempting to adapt this program for multi-survey plots on the printer it was found that the maximum number of print-characters contained in one print-line was not large enough to accommodate the number required by the multi-survey plots. Because of this, it was necessary to write the program for a computer plotter, rather than printer. The change from single to multiple survey tables necessitated a new input routine be established to handle the data from two surveys simultaneously.

4.1 THE PLOT

Subroutine TABLE was then written to produce a suitable table outline in which to plot the frequencies for the surveys' selected variables. Written for a general case, it produces only as many rows and columns for frequencies as are needed for each individual table. Control is returned to program BIVPLOT where the frequencies are then plotted and summary statistics for each survey can be calculated and plotted with each table. An example of this output is shown in Figure 28.

BIVARIATE TABLE FOR

WEIGHT	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	TTL	
267.50																																1
257.50																																
247.50																																
237.50																																
227.50																																
217.50																																
207.50																																
197.50																																
187.50																																
177.50																																
167.50																																
157.50																																
147.50																																
137.50																																
127.50																																
117.50																																
107.50																																
97.50																																
TOTAL	2	6	12	12	11	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
MIDVALUES FOR COLUMNS																																
1	1397.5	1417.5	1437.5	1457.5	1477.5	1497.5	1517.5	1537.5	1557.5	1577.5	1597.5	1617.5	1637.5	1657.5	1677.5	1697.5	1717.5	1737.5	1757.5	1777.5	1797.5	1817.5	1837.5	1857.5	1877.5	1897.5	1917.5	1937.5	1957.5	1977.5		
16																																
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27																																
28																																
29																																
30																																

ASSORTED STATISTICS MEAN ST DEV R REGRESSION EQUATIONS & STD ERROR
 HEIGHT 1677.25 116.46 .778 = (2.747)* HEIGHT 1297.736 71.93
 WEIGHT 138.16 32.42 .770 = (.220)* WEIGHT -231.347 71.93

Figure 27. Line Printer Output for a Single Survey from Program BARE BIVAR.

A BIVARIATE FREQUENCY TABLE FOR
SITTING HEIGHT AND STATURE
USAF MEN/USAF WOMEN

SITTING HEIGHT (CM)	STATURE (CM)																				TOTAL
	140.2	142.2	144.2	146.2	148.2	150.2	152.2	154.2	156.2	158.2	160.2	162.2	164.2	166.2	168.2	170.2	172.2	174.2	176.2	178.2	
104.2																					1
106.2																					1
108.2																					1
110.2																					1
112.2																					1
114.2																					1
116.2																					1
118.2																					1
120.2																					1
122.2																					1
124.2																					1
126.2																					1
128.2																					1
130.2																					1
132.2																					1
134.2																					1
136.2																					1
138.2																					1
140.2																					1
142.2																					1
144.2																					1
146.2																					1
148.2																					1
150.2																					1
152.2																					1
154.2																					1
156.2																					1
158.2																					1
160.2																					1
162.2																					1
164.2																					1
166.2																					1
168.2																					1
170.2																					1
172.2																					1
174.2																					1
176.2																					1
178.2																					1
TOTAL	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

USAF MEN ASSORTED STATISTICS	MEAN	ST DEV	R
STATURE (CM)	177.34	6.19	0.788
SITTING HEIGHT (CM)	93.10	3.18	0.788
USAF WOMEN ASSORTED STATISTICS	MEAN	ST DEV	R
STATURE (CM)	162.10	6.00	0.801
SITTING HEIGHT (CM)	85.60	3.17	0.801

REGRESSION EQUATIONS	
$SITTING HEIGHT (CM) = (1.535) \cdot STATURE (CM) + (34.31)$	
$STATURE (CM) = (0.404) \cdot SITTING HEIGHT (CM) + (21.54)$	
REGRESSION EQUATIONS	
$SITTING HEIGHT (CM) = (1.517) \cdot STATURE (CM) + (32.25)$	
$STATURE (CM) = (0.423) \cdot SITTING HEIGHT (CM) + (17.03)$	

STD ERROR	
3.81	
1.96	
STD ERROR	
3.60	
1.90	

DATE: 11/16/76
METRIC
PLOT: 48

Figure 28. Metric BIVPLOT Output.

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4.2 TABLE OF CONTENTS

Each bivariate table is also dated, numbered, and labeled as containing either METRIC or ENGLISH data. The numbering is done to keep track of the large volume of plots which are anticipated. Program CONTENTS was written to keep track of these plots. It uses the variable number of the sets of user-selected anthropometric variables with their respective plot numbers to produce a cross-reference table of contents for the plots. A sample cross-reference table is shown in Figure 29.

4.3 BIVPLOT MULTIPLE SURVEY TAPES

Data surveys used in generating bivariate tables are stored primarily on individual magnetic tapes. Handling two complete data survey tapes simultaneously, to generate a set of plots takes a considerable amount of computer time. The two surveys of interest have been the 1967 USAF MEN and the 1968 USAF WOMEN surveys. The primary interest in these surveys has been to see the relationship between sizes of men and women, to assist in the process of sizing uniforms and equipment to fit both males and females. To reduce input time for the plots using these surveys, 72 variables, which were common to both surveys were selected from the 204 variables in the men's survey and the 156 variables in the women's survey. These 72 selected variables were judged to be most useful for the sizing procedures. The common variables from the two survey tapes were combined into one tape containing all the pertinent information needed to run any combination of these variables over both surveys. In combining the tapes, all data were converted to metric units (cm/kg/years). The pertinent information for each variable included new range data based on the overall minimum and maximum values over both surveys, a plot step size factor, and a conversion factor for converting the metric unit to an English unit. Figure 30 shows the comparable variables from both surveys, and gives the range of values for each variable in the original unit of measurement. Figure 31 shows the data contained on the combined tape.

BIVARIATES FOR USAF MEN VS. WOMEN
(METRIC/ENGLISH PLOT NO.)

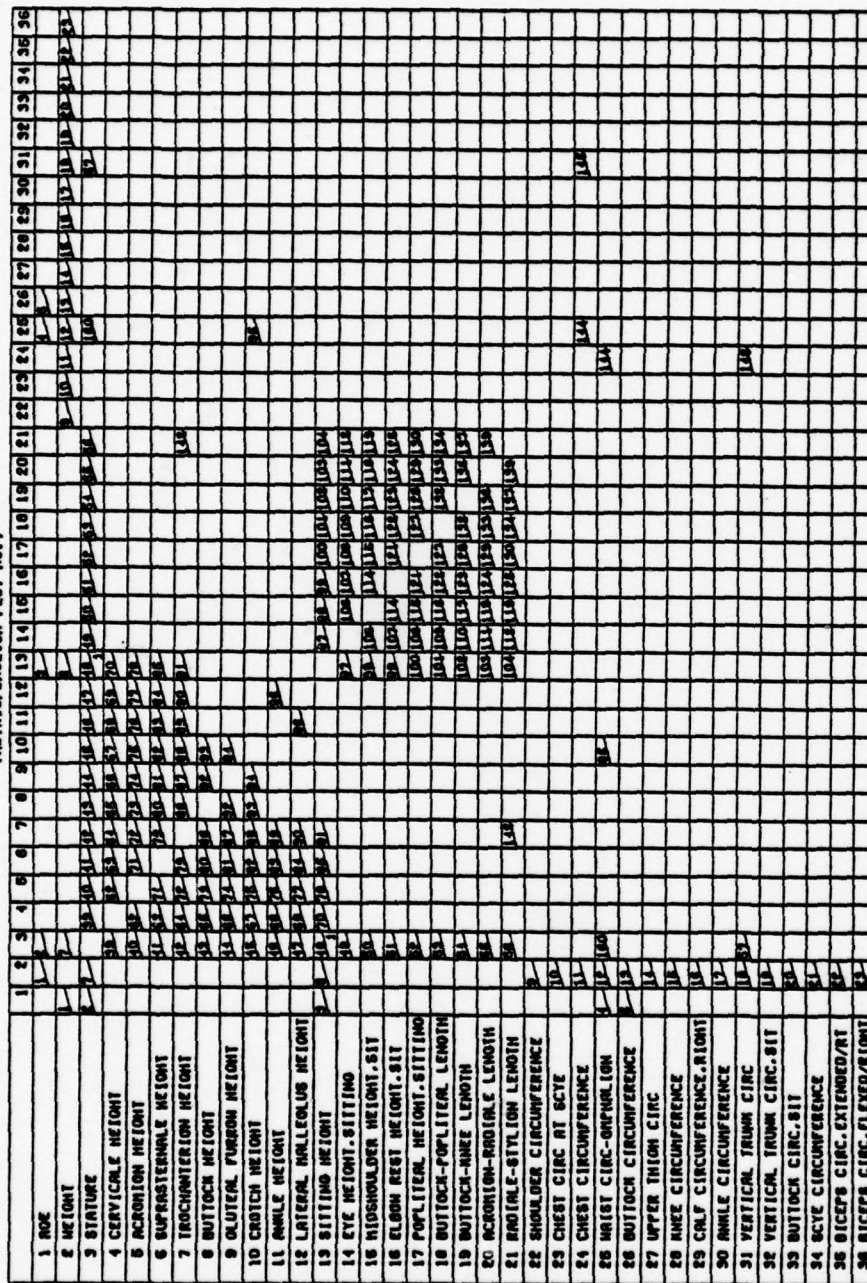


Figure 29. Table of Contents for 1967 USAF Men Vs. 1968 USAF Women
Plots; Plotted by Program Contents.

BIOMETERIES FOR USARF MEN VS. WOMEN
(METRIC/ENGLISH PLOT NO.)

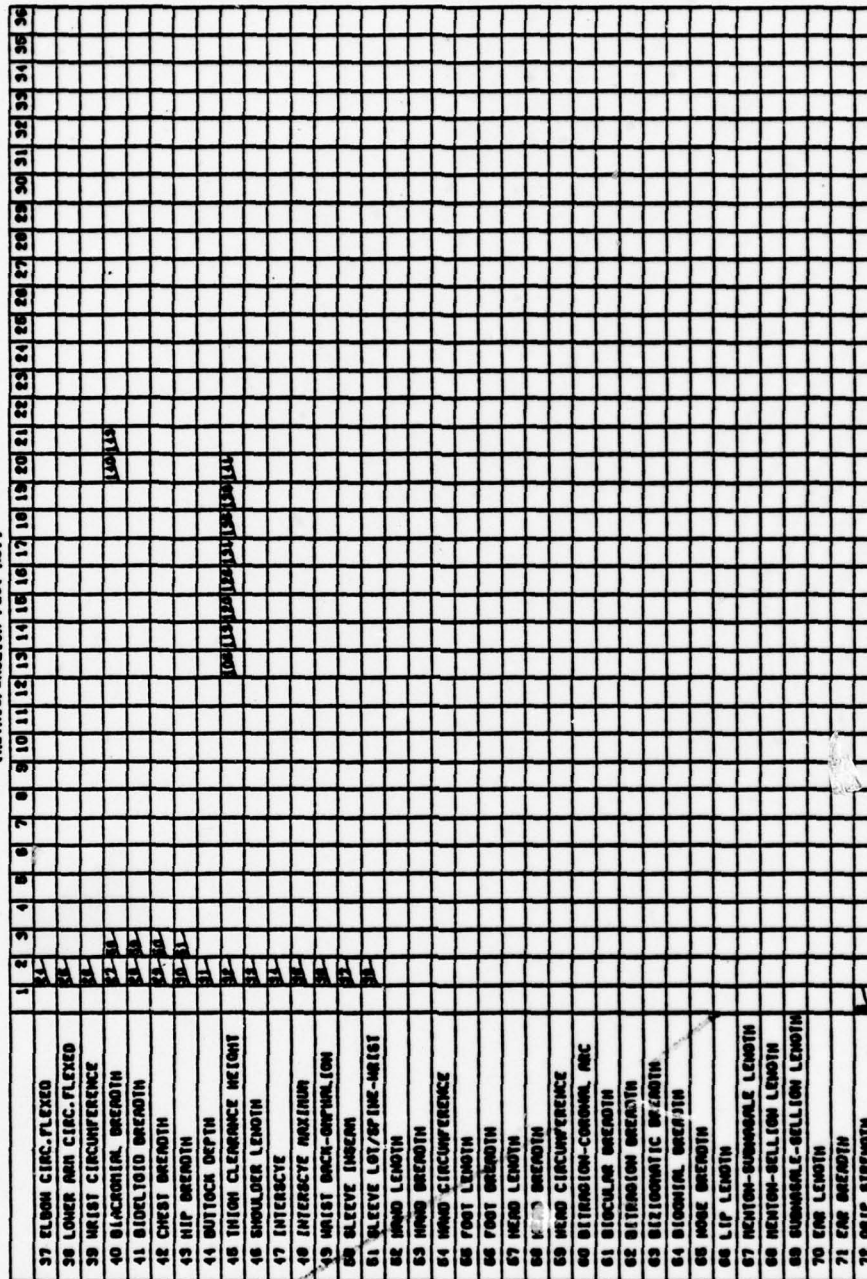
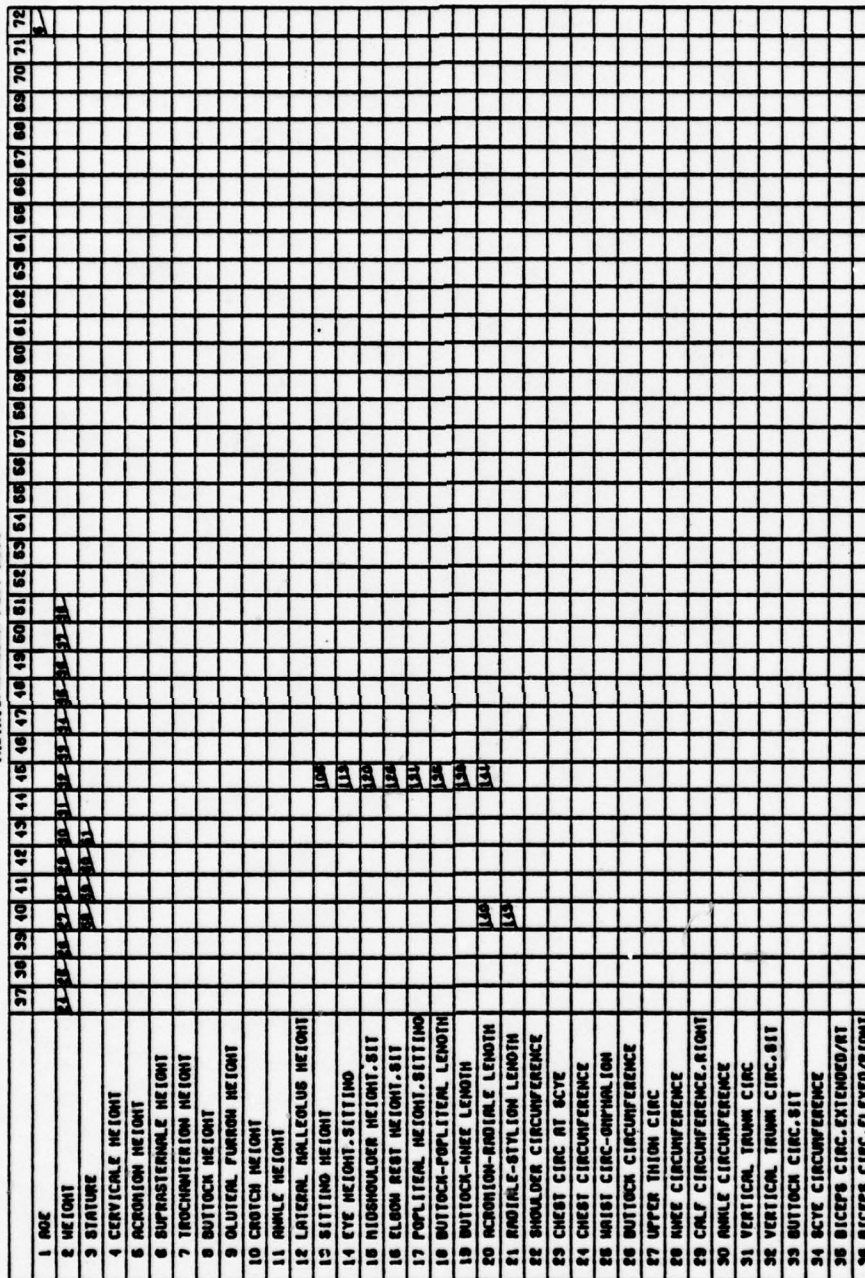


Figure 29 (Continued)

STANDARDIZATION FOR USARF MEN VS. WOMEN
(HEIGHT/ENROLLMENT PLOT NO.)



STANDARDIZATION FOR USE OF MEN VS. WOMEN
(METRIC/ENGLISH PLAT NO. 1)

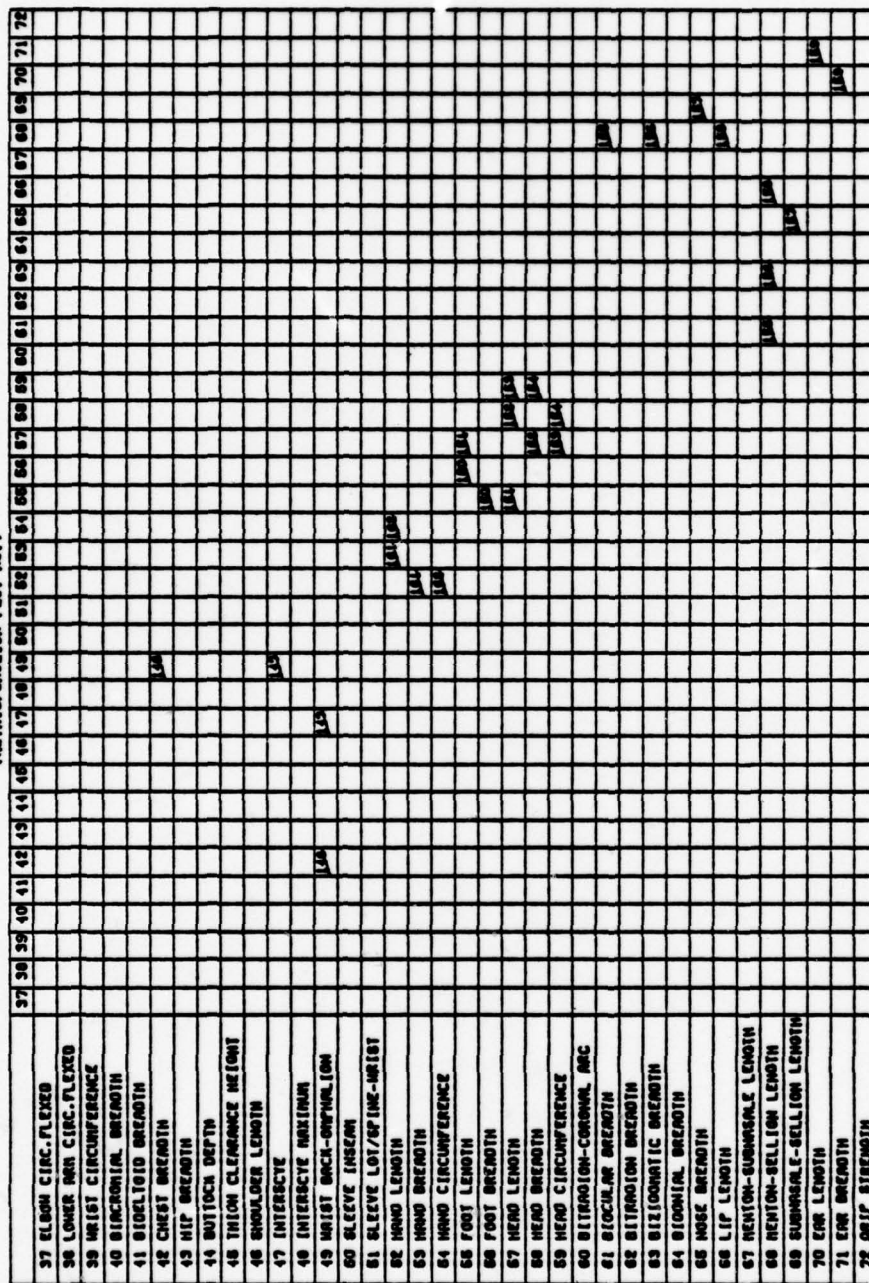


Figure 29 (Continued)

1967 USAF MEN					1968 USAF WOMEN				
NO.	SURVEY NO.	VARIABLE NAME	MINIMUM	MAXIMUM	SURVEY NO.	VARIABLE NAME	MINIMUM	MAXIMUM	
1	1	AGE	2100.00	5050.00	1	AGE	177.50	505.00	
2	2	WEIGHT	117.50	264.00	2	WEIGHT	82.50	200.00	
3	13	HEIGHT (STATURE)	1577.50	1972.00	7	STATURE	1442.50	1830.00	
4	14	CERVICAL HEIGHT	1342.50	1702.00	9	CERVICAL HEIGHT	1202.50	1500.00	
5	15	ACROMION HEIGHT	1277.50	1644.00	10	ACROMIAL HEIGHT	1142.50	1520.00	
6	19	SUPRATERNALE HGHT	1267.50	1623.00	11	SUPRATERNALE HGHT	1162.50	1506.00	
7	24	TROCHANTERION HGHT	787.50	1119.00	15	TROCHANTERIC HGHT	682.50	965.00	
8	23	BUTTOCK HEIGHT	767.50	1098.00	16	BUTTOCK HEIGHT	642.50	900.00	
9	25	GLUTEAL FURROW HGT	682.50	986.00	17	GLUTEAL FURROW HGT	582.50	864.00	
10	26	CROTCH HEIGHT	712.50	1035.00	19	CROTCH HEIGHT	602.50	875.00	
11	31	ANKLE HEIGHT	103.50	183.00	20	ANKLE HEIGHT	72.50	160.00	
12	132	LAT L MALLEOLUS HT	53.50	89.00	21	LAT L MALLEOLUS HT	47.50	87.00	
13	32	SITTING HEIGHT	867.50	1048.00	23	SITTING HEIGHT	752.50	964.00	
14	33	EYE HEIGHT/SITTING	682.50	910.00	24	EYE HEIGHT/SITTING	632.50	831.00	
15	34	MIDSHOULDER HT/SIT	537.50	746.00	25	MIDSHOULDER HT/SIT	502.50	722.00	
16	36	ELBOW REST HGT/SIT	152.50	351.00	27	ELBOW REST HEIGHT	142.50	295.00	
17	38	POPLITEAL HGT/SIT	362.50	512.00	28	POPLITEAL HEIGHT	332.50	471.00	
18	40	BUTTOCK-POPLITEAL	422.50	598.00	29	BUTTOCK-POPLIT L L	382.50	585.00	
19	39	BUTTOCK-KNEE LGTH	517.50	696.00	30	BUTTOCK-KNEE LGTH	482.50	664.00	
20	43	ACROMION-RADIALE L	271.50	393.00	31	ACROMION-RADIALE L	252.50	365.00	
21	45	RADIALE-STYLION LH	224.50	314.00	32	RADIALE-STYLION L	187.50	280.00	
22	67	SHOULDER CIRCUMF CE	997.50	1367.00	37	SHOULDER CIRCUMFER	862.50	1221.00	
23	68	CHEST CIRC AT SCYE	792.50	1243.00	38	CHEST CIRC AT SCYE	702.50	1035.00	
24	69	CHEST CIRCUMF ENCE	772.50	1214.00	39	BUST CIRCUMFERENCE	742.50	1139.00	
25	70	WAIST CIRC-OMPHAL N	677.50	1246.00	41	WAIST CIRCUMFERENCE	522.50	951.00	
26	72	BUTTOCK CIRCUMF CE	812.50	1244.00	44	HIP C-9 BLW WAIST	762.50	1201.00	
27	96	UPPER THIGH CIRCUM	452.50	759.00	45	UPPER THIGH CIRCUM	422.50	720.00	
28	98	KNEE CIRCUMFERENCE	312.50	482.00	46	KNEE CIRCUMFERENCE	302.50	457.00	
29	100	CALF CIRCUMF/RIGHT	297.50	452.00	47	CALF CIRCUM, RIGHT	262.50	445.00	
30	102	ANKLE CIRCUMF ENCE	181.50	267.00	49	ANKLE CIRCUMFERENCE	172.50	256.00	
31	74	VERTICAL TRUNK CIR	1422.50	1975.00	50	VERTICAL TRUNK CIR	1342.50	1782.00	
32	75	VERT TRUNK CIR/SIT	1367.50	1856.00	51	VERTICAL TRK C,SIT	1322.50	1705.00	
33	73	BUTTOCK CIRCUM/SIT	867.50	1411.00	52	BUTTOCK CIRC, SIT	842.50	1284.00	
34	103	SCYE CIRCUMFERENCE	402.50	594.00	53	SCYE CIRCUMFERENCE	282.50	490.00	
35	104	BICEPS C-EXTENDED/RT	227.50	388.00	55	BICEPS C,RELAXED,R	192.50	374.00	
36	106	BICEPS C-FLEXED/RT	252.50	408.00	56	BICEPS C,FLEXED, R	192.50	390.00	
37	109	ELBOW CIRC-FLEXED	258.50	369.00	59	ELBOW CIRC, FLEXED	212.50	358.00	
38	111	LOWER ARM C-FLEXED	241.50	354.00	61	FOREARM C, FLEXED	192.50	328.00	
39	112	WRIST CIRCUMF ENCE	150.50	208.00	62	WRIST CIRCUMFERENCE	122.50	176.00	
40	50	BIACROMIAL BREADTH	337.50	474.00	63	BIACROMIAL BREADTH	307.50	410.00	
41	51	BIOELTIOID BREADTH	357.50	567.00	64	BIOELTIOID BREADTH	342.50	501.00	
42	52	CHEST BREADTH	257.50	415.00	65	CHEST BREADTH	222.50	359.00	
43	55	HIP BREADTH	282.50	446.00	68	HIP BREADTH	282.50	441.00	
44	64	BUTTOCK DEPTH	170.50	338.00	77	BUTTOCK DEPTH	152.50	306.00	
45	65	THIGH CLEARANCE HT	124.50	217.00	78	THIGH CLEARANCE	87.50	169.00	
46	118	SHOULDER LENGTH	131.50	217.00	79	SHOULDER LENGTH	112.50	188.00	
47	120	INTERSCYE	270.50	514.00	82	INTERSCYE	272.50	442.00	
48	121	INTERSCYE MAXIMUM	492.50	713.00	83	INTERSCYE, MAXIMUM	372.50	605.00	
49	124	WAIST BACK-OMPHAL N	402.50	563.00	85	WAIST BACK	332.50	481.00	
50	49	SLEEVE INSEAM	397.50	578.00	87	SLEEVE INSEAM	362.50	535.00	
51	115	SLVE L/SPINE-WRIST	747.50	1045.00	90	SPINE-TO-WRIST LTH	672.50	912.00	
52	134	HAND LENGTH	166.50	222.00	91	HAND LENGTH	152.50	220.00	
53	136	HAND BR/METACARPLE	75.50	102.00	92	HAND BREADTH	60.50	88.00	
54	138	HAND C/METACARPALE	143.50	247.00	93	HAND CIRCUMFERENCE	147.50	215.00	
55	125	FOOT LENGTH	231.50	313.00	94	FOOT LENGTH	207.50	276.00	
56	127	FOOT BREADTH	83.50	117.00	95	FOOT BREADTH	67.50	110.00	
57	150	HEAD LENGTH	174.50	226.00	96	HEAD LENGTH	162.50	207.00	
58	156	HEAD BREADTH	138.50	176.00	97	HEAD BREADTH	122.50	171.00	
59	141	HEAD CIRCUMFERENCE	526.50	620.00	98	HEAD CIRCUMFERENCE	497.50	617.00	
60	144	BITRAGION-CORONAL	320.50	402.00	112	BITRAGION-CORONAL	287.50	392.00	
61	162	BIOCLULAR BREADTH	77.50	108.00	113	BIOCLULAR BREADTH	78.50	112.00	
62	158	BITRAGION BREADTH	123.50	161.00	115	BITRAGION BREADTH	112.50	152.00	
63	159	BIZYGOMATIC BR DTH	123.50	159.00	116	BIZYGOMATIC BRDTH	108.50	149.00	
64	160	BIGONIAL BREADTH	94.50	142.00	117	BIGONIAL BREADTH	80.50	122.00	
65	165	NOSE BREADTH	26.50	51.00	118	NASAL BREADTH	22.50	46.00	
66	166	LIP LENGTH	38.50	66.00	119	LIP LENGTH	30.50	58.00	
67	171	MENTON-SUBNASALE L	52.50	89.00	120	MENTON-SUBNASALE L	38.50	75.00	
68	172	MENTON-NASAL ROOT	97.50	143.00	121	MENTON-SELLION LTH	86.50	128.00	
69	168	SUBNASALE-NASAL RT	38.50	64.00	122	SUBNASALE-SELLION	30.50	61.00	
70	154	EAR LENGTH	48.50	83.00	123	EAR LENGTH	34.50	69.00	
71	153	EAR BREADTH	26.50	51.00	124	EAR BREADTH	18.50	42.00	
72	12	GRIP STRENGTH	32.50	86.00	125	GRIP STRENGTH	9.50	53.00	

Figure 30. Survey Variable Names, Numbers and Ranges from the Individual Survey Tapes.

```

***** A COMBINED TAPE FOR USAF WOMEN(1960), AND USAF MEN(1967) *****
REC 0001.. 72 VARIABLES USAF MEN/USAF WOMEN
REC 0002.. (13,1X,6A4,13,3F9.2,F11.7,3X,2A4)
REC 0003.. (14,19F4.1,/, (20F4.1))
REC 0004.. 1 AGE 3 10-50 57.00 1.50 1.0000000 (YR)(YR)
REC 0005.. 2 HEIGHT 6 37.42 119.75 3.00 2.2046223 (KG)(LB)
REC 0006.. 3 STATURE 7 144.25 197.20 2.00 0.3937008 (CH)(IN)
REC 0007.. 4 CERVICAL HEIGHT 16 120.25 170.20 2.00 0.3937008 (CH)(IN)
REC 0008.. 5 ACROMION HEIGHT 15 114.25 164.40 2.00 0.3937008 (CH)(IN)
REC 0009.. 6 SUPRASTERNAL HEIGHT 20 116.25 162.30 2.00 0.3937008 (CH)(IN)
REC 0010.. 7 TROCHANTERION HEIGHT 20 68.25 111.90 1.50 0.3937008 (CH)(IN)
REC 0011.. 8 BUTTOCK HEIGHT 14 64.25 109.80 2.00 0.3937008 (CH)(IN)
REC 0012.. 9 GLUTEAL FURROW HEIGHT 21 58.25 98.60 1.50 0.3937008 (CH)(IN)
REC 0013.. 10 CROICH HEIGHT 13 60.25 103.50 1.50 0.3937008 (CH)(IN)
REC 0014.. 11 ANKLE HEIGHT 12 7.25 18.30 0.40 0.3937008 (CH)(IN)
REC 0015.. 12 LATERAL MALLEOLUS HEIGHT 24 4.75 8.90 0.20 0.3937008 (CH)(IN)
REC 0016.. 13 SITTING HEIGHT 14 75.25 104.80 1.00 0.3937008 (CH)(IN)
REC 0017.. 14 EYE HEIGHT, SITTING 18 63.25 91.00 1.00 0.3937008 (CH)(IN)
REC 0018.. 15 MIDSHOULDER HEIGHT, SIT 22 50.25 74.60 1.00 0.3937008 (CH)(IN)
REC 0019.. 16 ELBOW REST HEIGHT, SIT 21 14.25 35.10 0.80 0.3937008 (CH)(IN)
REC 0020.. 17 POPLITEAL HEIGHT, SITTING 24 33.25 51.20 0.60 0.3937008 (CH)(IN)
REC 0021.. 18 BUTTOCK-POPLITEAL LENGTH 24 38.25 59.80 0.80 0.3937008 (CH)(IN)
REC 0022.. 19 BUTTOCK-KNEE LENGTH 19 48.25 69.60 0.80 0.3937008 (CH)(IN)
REC 0023.. 20 ACROMION-RADIAL LENGTH 23 25.25 39.30 0.60 0.3937008 (CH)(IN)
REC 0024.. 21 RADIAL-STYLE LENGTH 22 18.75 31.40 0.60 0.3937008 (CH)(IN)
REC 0025.. 22 SHOULDER CIRCUMFERENCE 22 86.25 136.70 2.00 0.3937008 (CH)(IN)
REC 0026.. 23 CHEST CIRC AT SCYE 18 70.25 124.30 2.00 0.3937008 (CH)(IN)
REC 0027.. 24 CHEST CIRCUMFERENCE 19 74.25 121.40 2.00 0.3937008 (CH)(IN)
REC 0028.. 25 WAIST CIRC-OMPHALION 20 52.25 124.60 2.00 0.3937008 (CH)(IN)
REC 0029.. 26 BUTTOCK CIRCUMFERENCE 21 76.25 124.40 2.00 0.3937008 (CH)(IN)
REC 0030.. 27 UPPER THIGH CIRC 16 42.25 75.90 1.50 0.3937008 (CH)(IN)
REC 0031.. 28 KNEE CIRCUMFERENCE 18 30.25 48.20 0.60 0.3937008 (CH)(IN)
REC 0032.. 29 CALF CIRCUMFERENCE, RIGHT 24 25.25 45.20 0.80 0.3937008 (CH)(IN)
REC 0033.. 30 ANKLE CIRCUMFERENCE 19 17.25 26.70 0.40 0.3937008 (CH)(IN)
REC 0034.. 31 VERTICAL TRUNK CIRC 19 134.25 197.50 2.50 0.3937008 (CH)(IN)
REC 0035.. 32 VERTICAL TRUNK CIRC, SIT 23 132.25 185.60 2.00 0.3937008 (CH)(IN)
REC 0036.. 33 BUTTOCK CIRC, SIT 16 84.25 141.10 2.00 0.3937008 (CH)(IN)
REC 0037.. 34 SCYE CIRCUMFERENCE 18 28.25 59.40 1.50 0.3937008 (CH)(IN)
REC 0038.. 35 BICEPS CIRC, EXTENDED/RT 23 19.25 38.80 0.80 0.3937008 (CH)(IN)
REC 0039.. 36 BICEPS CIRC, FLEXED/RIGHT 24 19.25 40.80 0.80 0.3937008 (CH)(IN)
REC 0040.. 37 ELBOW CIRC, FLEXED 17 21.25 36.90 0.60 0.3937008 (CH)(IN)
REC 0041.. 38 LOWER ARM CIRC, FLEXED 21 19.25 35.40 0.60 0.3937008 (CH)(IN)
REC 0042.. 39 WRIST CIRCUMFERENCE 19 12.25 20.80 0.40 0.3937008 (CH)(IN)
REC 0043.. 40 BIACROMIAL BREADTH 18 30.75 47.40 0.60 0.3937008 (CH)(IN)
REC 0044.. 41 BIELTROID BREADTH 17 34.25 56.70 0.80 0.3937008 (CH)(IN)
REC 0045.. 42 CHEST BREADTH 13 22.25 41.50 0.80 0.3937008 (CH)(IN)
REC 0046.. 43 HIP BREADTH 11 28.25 44.60 0.60 0.3937008 (CH)(IN)
REC 0047.. 44 BUTTOCK DPTH 13 15.25 33.80 0.80 0.3937008 (CH)(IN)
REC 0048.. 45 THIGH CLEARANCE HEIGHT 22 8.75 21.70 0.80 0.3937008 (CH)(IN)
REC 0049.. 46 SHOULDER LENGTH 15 11.25 21.70 0.40 0.3937008 (CH)(IN)

```

Figure 31. Combined Tape for Input to BIVPLOT.

REC 0051..	47 INTERSCYE	9	27.05	51.40	1.00	0.3937008	(CM) (IN)
REC 0052..	48 INTERSCYE MAXIMUM	17	37.25	71.30	1.50	0.3937008	(CM) (IN)
REC 0053..	49 MAIST BACK-OMPHALION	20	33.25	56.30	0.80	0.3937008	(CM) (IN)
REC 0054..	50 SLEEVE INSEAM	13	36.25	57.80	0.80	0.3937008	(CM) (IN)
REC 0055..	51 SLEEVE LGT/SPINE-WRIST	22	67.25	104.50	1.50	0.3937008	(CM) (IN)
REC 0056..	52 HAND BREADTH	11	15.25	22.20	0.40	0.3937008	(CM) (IN)
REC 0057..	53 HAND BREADTH	12	6.45	10.20	0.20	0.3937008	(CM) (IN)
REC 0058..	54 HAND CIRCUMFERENCE	18	14.75	24.70	0.40	0.3937008	(CM) (IN)
REC 0059..	55 FOOT LENGTH	11	20.75	31.30	0.40	0.3937008	(CM) (IN)
REC 0060..	56 FOOT BREADTH	12	6.75	11.70	0.20	0.3937008	(CM) (IN)
REC 0061..	57 HEAD LENGTH	11	16.25	22.60	0.40	0.3937008	(CM) (IN)
REC 0062..	58 HEAD BREADTH	12	12.25	17.60	0.20	0.3937008	(CM) (IN)
REC 0063..	59 HEAD CIRCUMFERENCE	18	49.75	62.00	0.60	0.3937008	(CM) (IN)
REC 0064..	60 BITRAGON-CORONAL ARC	21	28.75	40.20	0.40	0.3937008	(CM) (IN)
REC 0065..	61 BITRAGON BREADTH	16	7.75	11.20	0.20	0.3937008	(CM) (IN)
REC 0066..	62 BITRAGON BREADTH	17	11.25	16.10	0.20	0.3937008	(CM) (IN)
REC 0067..	63 BITRAGON BREADTH	19	10.85	15.90	0.20	0.3937008	(CM) (IN)
REC 0068..	64 BITRAGON BREADTH	16	8.05	14.20	0.40	0.3937008	(CM) (IN)
REC 0069..	65 NOSE BREADTH	12	2.25	5.10	0.20	0.3937008	(CM) (IN)
REC 0070..	66 LIP LENGTH	10	3.05	6.60	0.20	0.3937008	(CM) (IN)
REC 0071..	67 MENTON-SUBNASALE LENGTH	23	3.85	8.90	0.20	0.3937008	(CM) (IN)
REC 0072..	68 MENTON-SELLION LENGTH	21	8.65	14.30	0.20	0.3937008	(CM) (IN)
REC 0073..	69 SUBNASALE-SELLION LENGTH	24	3.05	6.40	0.20	0.3937008	(CM) (IN)
REC 0074..	70 EAR LENGTH	10	3.45	6.30	0.20	0.3937008	(CM) (IN)
REC 0075..	71 EAR BREADTH	11	1.85	5.10	0.20	0.3937008	(CM) (IN)
REC 0076..	72 GRIP STRENGTH	13	9.50	86.00	3.00	2.2046223	(KG) (LB)
REC 0077..	15 415 81217114781351417	911	866 736	807 130	73 306	802 847 248 409 465 581	
REC 0078..	343 275116811221125 395 974	559	359 359	221168216271084	466 206 306 311 287 169		
REC 0079..	407 485 344 339 260 156 148	418	592 462	490 915 188 89 216 260	94 192 152 563		
REC 0080..	347 89 137 137 111 36 53	78	132 55	70 38 490			
REC 0081..	16 415 771176615141271444	942	892 798	837 148 74 314	788 609 208 415 495 605		
REC 0082..	329 2681151026 975 941 957 578	384	373	223170115851042 487	326 332 308 289 180		
REC 0083..	404 477 336 343 222 165 165	426	622 456	488 899 193 92 221	249 101 202 156 580		
REC 0084..	341 91 143 141 121 39 54	74	136 57	65 36 520			
REC 0085..	17 425 7801834156614861488	948	889 804	830 130 76 369	859 671 278 439 515 629		
REC 0086..	325 2611142 997 931 805 981	591	399 393	233175416961068	466 297 312 310 300 177		
REC 0087..	427 500 337 350 241 152 173	454	613 467	479 928 187 92 228	268 101 190 161 569		
REC 0088..	350 91 156 149 117 39 55	66	121 56	76 40 530			
REC 0089..	18 445 8301779153614551464	946	926 833	839 136 72 332	802 640 239 442 501 616		
REC 0090..	335 282114110571034 9331043	618	380 367	215173016521155	442 326 349 332 294 185		
REC 0091..	408 487 349 382 258 153 160	422	576 461	499 902 186 92 214	272 97 195 148 557		
REC 0092..	325 91 145 138 106 33 49	66	121 52	68 40 510			
REC 0093..	19 425 95318601643154615401018	996	892 911	158 72 939	824 668 275 474 531 647		
REC 0094..	346 2951245115211510201038	615	402 385	224174216701155	491 330 344 339 324 182		
REC 0095..	421 515 372 377 274 166 179	442	643 469	507 966 200 98 232	288 106 206 159 596		
REC 0096..	357 92 151 141 116 37 48	71	124 50	68 39 620			
REC 0097..	20 395 95319561669160716051001	963	875 896	160 761048	900 714 289 474 530 630		
REC 0098..	350 279124511051066 8451016	582	409 392	244186417551077	492 344 357 342 322 204		
REC 0099..	451 520 369 369 240 156 178	488	655 512	504 937 210 98 229	297 96 221 160 618		
REC 0100..	394 100 152 155 117 41	59	80 143	64 79 43	640		

Page 2 of 2

Figure 31 (Continued)

In a like manner, the Health Examination Survey of men and women were put on another tape for their analyses.

4.4 EQUALIZING SAMPLE SIZES

In order to make these multiple bivariate plots (multi-bivplots) as useful as possible, the sample sizes were equalized. It was decided that only the first 2000 subjects from the 1967 USAF Male survey would be used, and datasets for 95 subjects would be added to the 1905 subjects on the 1968 USAF Female survey. These 95 datasets were chosen at random using a UDRI-written program, RANDOM, which, in turn, employed a random number generating routine from the CDC 6600 computer system. The original 2420-subject data values from the 1967 survey and the 1905-subject data values from the 1968 survey were used to calculate the summary statistics.

4.5 SUMMARY

To date one English and 162 metric plots have been generated from the 1967 versus 1968 USAF surveys tape. Each plot is approximately 14"x10" in size and is plotted using a .2 mm India ink pen on the offline CALCOMP plotter at the ASD Computer Center (Building 676). Plot tapes are generated on the CDC 6600 computer system at Building 676 using the CDC 1700 remote job entry terminal at Building 441. These plot tapes are then read by the CALCOMP 780 magnetic tape unit and plotted with a CALCOMP 763 digital incremental zip-mode plotter. This route has offered the best resolution and quality of output. However, because of the time required to generate these plots on the CALCOMP plotter, only ten plots can be produced a day. Once the plots have been produced, they are reduced to 8½"x11" inch size on a reducing copy machine in Building 676 for their general use.

The original and primary use for these plots by AMRL has been for the recent series of chemical warfare clothing and personal equipment sizing and fit tests. These multi-bivplots have been an aid in sizing face respirators, protective garments, and gloves for both men and women in the ground forces.

Further multi-bivplots are expected to be produced and used in the future. Program BIVPLOT, however, is not fully documented and further changes are to be made to BIVPLOT during the next contract period. A series of these bivariate plots will be published in 1977 along with a more extensive documentation of program BIVPLOT and its accompanying subroutines. At that time the input formats for BIVPLOT will also be documented in full.

SECTION 5

BIOSTEREOMETRIC DATA

This section contains the analysis of a new set of data obtained during this contract period. This set of data was collected for AMRL/HED by R. E. Herron et al., of the Biostereometrics Laboratory at the Texas Institute for Rehabilitation and Research, for the purpose of collecting mass distribution measurements for six anatomical specimens using biostereometrics (see Reference 8). This was done in conjunction with Chandler et al. (see Reference 9) who used the pendulum method to gather mass distribution data on these same specimens.

5.1 HERRON'S BIOSTEREOMETRIC DATA

Herron's biostereometric cadaver data were obtained from AMRL during the contract period covered in this report, and some preliminary statistical analyses were performed on the data using program HER1. The substance of Herron's data was published in AMRL-TR-75-18 pages 56-193 (Reference 8).

Statistical analyses performed on these data have been the following:

- A. New densities, called DENSITY 4, were calculated using Herron's volumes and measured cadaver weights, as reported in the Department of Transportation (DOT) report DOT HS-801 430, for each segment.
- B. A mean DENSITY 4 was calculated for each segment.
- C. Segment weights were recalculated using the DENSITY 4 mean value and Herron's volumes.

5.2 INPUT

Input for HER1 consisted of: a numbered variable name card for each segment, using a format of (I4, 1X, 3A4); a card for each segment with the DOT reported densities and weights for each of the six cadavers, using format

(I2, 2X, 6(F6.4, F6.1)); tables 9, 21, 33, 45, 57, and 69 from Herron's data, each followed by a blank card. Format information for Herron's data is shown in Figure 32.

5.3 SUMMARY

Figure 33 shows the general flow of program HER1, which was used to perform the original data analyses. Figures 34, 35, and 36 show the DOT input, the first two tables of the Herron input, and the output for the first three cadaver segments respectively.

No further analyses of the biostereometric data has been planned, pending discussions with Dr. Herron at the Biostereometrics laboratory regarding his data.

Each punched card corresponds to one line of the data in the tables. The first two numbers of the cards represent the table number and the data line of that table, respectively. The numbers that follow are the same as those of the data in the tables. (Disregard the last 8 digits of each pink card.)

For example a card with: 34 19 3 1206388.6 1491387.0 3717724.4

is from the 34th table, the 19th data line (column headings, titles, and subtitles were not numbered) and the next 4 fields are the data.

Twelve different formats were used for the cards:

Format #	Table #
1	Table 1, lines 1-16
2	Table 1, lines 17-22
3	Tables 2-7, odd lines
4	Tables 2-7, even lines
5	Table 8
6	Tables 9,13,17,21,25,29,33,37,41,45,49,53,57,61,65,69,73,77
7	Tables 10-80, except those listed above
8	Tables 81-116, lines 1,4,7,10,13,16,19,22,25
9	Tables 81-116, all other lines
10	Tables 117,119,121
11	Tables 118,120,122
12	All table titles, subtitles, column headings

The Fortran coding for the above formats is as follows:

Format (1)	I3,I6,3X,I2,F27.3,2F16.3
Format (2)	I3,I6,3X,I2,F27.3,F16.3,F6.3,F10.3,F6.3
Format (3)	I3,I6,3X,I2,F10.1,F12.2,F13.1,F10.1,F12.1
Format (4)	I3,I6,25X,F15.1,F10.1,F12.1
Format (5)	I3,I6,3X,I2,F17.1,F6.1,F7.1,F13.1,F6.1,F7.1
Format (6)	I3,I6,3X,I2,F10.3,F10.1,F9.2,F11.1,F8.1,F9.1
Format (7)	I3,I6,3X,I2,F17.1,F20.1,F20.1
Format (8)	I3,I6,3X,I2,F17.10,2F20.10
Format (9)	I3,I6,5X,F17.10,2F20.10
Format (10)	I3,I6,3X,I2,F14.1,F17.1,F16.1,F14.1
Format (11)	I3,I6,3X,I2,F12.2,F14.2,F16.2,F15.2
Format (12)	20A4

Figure 32. Format Information for Herron's Data (Reference 8).

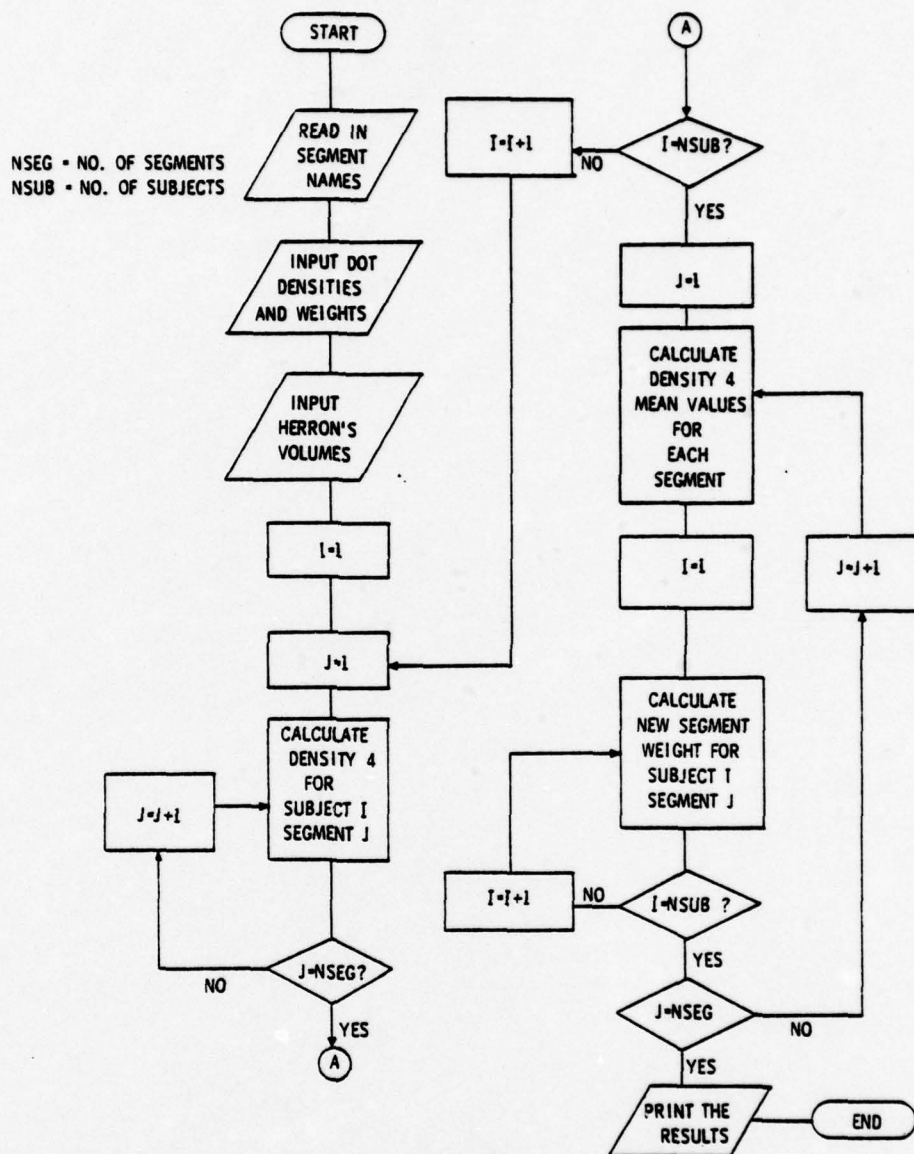


Figure 33. General Flow of Program HER1.

1	HEAD												
2	R UPPER ARM												
3	R FOREARM												
4	R HAND												
5	L UPPER ARM												
6	L FOREARM												
7	L HAND												
8	R THIGH												
9	R CALF												
10	R FOOT												
11	L THIGH												
12	L CALF												
13	L FOOT												
14	TORSO												
15	WHOLE BODY												
1	1055	4025	1040	4152	1090	4821	1052	3358	1055	4205	1030	3471	
2	1007	1794	1003	1941	981	2248	981	1530	1012	1012	957	1719	
3	1001	971	1017	1293	1035	1024	1051	790	1000	1011	1029	985	
4	1103	303	1062	490	1037	552	1077	320	1080	355	1050	302	
5	1033	1807	1004	2103	508	2404	1002	1530	1010	1500	1025	1019	
6	1094	1002	1050	1170	1037	1418	1029	819	1001	927	1007	1149	
7	1091	324	1003	409	1072	457	1075	320	1080	351	1048	332	
8	1021	3001	1012	1294	1021	5710	1034	3123	1022	9012	995	5332	
9	1062	2152	1054	2876	1073	3779	1052	2251	1057	2744	1057	2282	
10	1025	771	1024	1029	1020	530	1054	710	1057	459	1107	057	
11	1033	5839	1013	8082	1020	9399	1017	3000	1001	0090	1030	5733	
12	1047	2248	1049	3039	1064	3794	1074	1020	1041	2510	1053	2343	
13	1104	807	1038	1074	1092	574	1057	720	1053	703	1065	671	
14	833	3001	877	4100	911	4014	792	2002	821	2000	857	11202	
	58700		76150		89150		50620		50000		50340		
SUBJECT 1 SUBJECT 2 SUBJECT 3 SUBJECT 4 SUBJECT 5 SUBJECT 6													

Figure 34. Input from Report DOT-HS-801:430 Variable Names and Density/Weight Values for Each Segment (Reference 9).

TABLE 19			SUBJECT 1				DENSITY 1.0000100		
MASS AND CENTER OF GRAVITY (UNITS: C.G.S.)									
			DENSITY	MASS	MASS	A C.G.	Y C.G.	Z C.G.	
SEGMENTS									
9	1	1	1.000	4541.0	0.47	-0.7	2.0	56.9	00000200
9	2	2	1.000	20901.1	43.06	-0.3	-1.1	21.8	00000300
9	3	3	1.000	0174.2	10.84	0.5	1.0	-11.1	00000700
9	4	4	1.000	1920.7	3.03	21.6	-5.2	28.1	00000300
9	5	5	1.000	983.1	1.54	33.8	-4.4	5.4	00000200
9	6	6	1.000	410.2	0.00	33.3	-0.4	-14.0	00001000
9	7	7	1.000	2017.4	3.23	-23.0	-4.6	28.9	00000100
9	8	8	1.000	941.4	1.51	-31.8	-2.7	5.9	00001200
9	9	9	1.000	347.9	0.30	-44.3	0.9	-12.8	00000200
9	10	10	1.000	0200.9	9.93	12.0	1.0	-30.5	00001400
9	11	11	1.000	2212.4	3.54	10.1	2.2	-71.4	00001500
9	12	12	1.000	311.5	1.30	17.5	8.8	-100.2	00001000
9	13	13	1.000	5550.3	9.52	-10.4	1.4	-31.0	00001700
9	14	14	1.000	2204.0	3.53	-13.7	2.7	-71.5	00001300
9	15	15	1.000	171.0	1.23	-15.4	3.7	-59.9	00000900
9	16	16	1.000	33075.3	53.90	-0.4	-0.7	15.2	00002000
PARTS									
9	17	1	1.000	17710.3	60.00	-0.5	-0.4	19.7	00002200
9	18	2	1.000	3300.0	5.26	25.7	-4.3	10.2	00002300
9	19	3	1.000	3307.1	5.29	-20.1	-3.2	17.0	00002400
9	20	4	1.000	9230.6	14.77	11.5	2.0	-46.5	00002500
9	21	5	1.000	3920.3	14.29	-11.7	2.3	-47.5	00002600
WHOLE BODY									
9	22	1	1.000	62480.4	100.00	0.0	0.0	0.0	00002800

TABLE 21			SUBJECT 2				DENSITY 1.0037400		
MASS AND CENTER OF GRAVITY (UNITS: C.G.S.)									
			DENSITY	MASS	MASS	A C.G.	Y C.G.	Z C.G.	
SEGMENTS									
21	1	1	1.000	4190.4	5.33	0.1	1.8	62.0	00037800
21	2	2	1.000	34001.3	44.07	0.0	-1.3	24.9	00037900
21	3	3	1.000	8150.3	10.37	0.0	0.7	-9.0	00038000
21	4	4	1.000	2109.5	2.63	24.0	-3.0	30.0	00038100
21	5	5	1.000	1103.3	1.48	34.5	-2.4	4.9	00038200
21	6	6	1.000	494.1	0.63	42.3	0.7	-17.1	00038300
21	7	7	1.000	2328.4	2.90	-24.1	-5.3	33.5	00038400
21	8	8	1.000	1100.0	1.47	-20.1	-3.8	0.1	00038500
21	9	9	1.000	422.0	0.54	-41.1	-0.5	-15.0	00038600
21	10	10	1.000	7532.4	5.84	11.0	1.7	-31.5	00038700
21	11	11	1.000	2067.0	3.07	19.5	4.2	-77.0	00038800
21	12	12	1.000	1050.3	1.39	14.0	9.2	-109.9	00038900
21	13	13	1.000	5278.9	10.52	-0.7	1.2	-30.3	00039000
21	14	14	1.000	3010.1	3.83	-13.0	3.5	-77.0	00039100
21	15	15	1.000	1113.3	1.42	-12.9	10.3	-110.2	00039200
21	16	16	1.000	42317.9	54.44	0.0	-1.1	18.5	00039300
PARTS									
21	17	1	1.000	47034.3	59.77	0.0	-0.9	22.4	00039400
21	18	2	1.000	3709.4	4.79	29.7	-2.5	16.4	00039500
21	19	3	1.000	3911.1	4.97	-29.5	-4.4	20.7	00039600
21	20	4	1.000	11500.4	14.70	12.0	3.0	-50.3	00039700
21	21	5	1.000	12403.6	15.77	-11.0	2.0	-45.3	00039800
WHOLE BODY									
21	22	1	1.000	70889.7	100.00	0.0	0.0	0.0	00040000

Figure 35. First Two Tables of Herron's Data Input for HER1.

DENSITY DOT AND OLD WEIGHT ARE FROM DOT HS-601 430
 HERRON'S VOLUMES ARE THE MASS VALUES FROM HIS MASS AND CENTER OF
 GRAVITY TABLES WITH DENSITY=1.0
 DENSITY 4 WAS CALCULATED FROM THE OLD WEIGHTS AND HERRON'S VOLUMES
 THE NEW WEIGHTS WERE CALCULATED FROM THE DENSITY 4 MEAN VALUES AND
 HERRON'S VOLUMES

SUBJECT	DENSITY		HERRON'S VOLUME	OLD WEIGHT	NEW WEIGHT
	DOT	DENSITY 4			
1	1.0550	0.9900	4041.0	4025.0	4079.7
2	1.0460	0.9844	4196.4	4152.0	4230.0
3	1.0500	1.0591	4552.1	4621.0	4545.7
4	1.0520	1.0340	3235.1	3458.0	3200.1
5	1.0550	0.9842	4154.0	4105.0	4194.3
6	1.0300	0.9308	3517.0	3471.0	3551.3

THE HEAD DENSITY 4 MEAN VALUE IS 1.0090

SUBJECT	DENSITY		HERRON'S VOLUME	OLD WEIGHT	NEW WEIGHT
	DOT	DENSITY 4			
1	1.0070	0.9311	1926.7	1794.0	1764.4
2	1.0030	0.9201	2109.5	1941.0	1931.8
3	0.9810	0.9187	2440.9	2248.0	2240.7
4	0.9030	0.8345	1730.8	1538.0	1592.3
5	1.0120	0.9225	1907.4	1815.0	1801.0
6	0.9970	0.9174	1873.7	1715.0	1715.8

THE R UPPER ARM DENSITY 4 MEAN VALUE IS 0.9157

SUBJECT	DENSITY		HERRON'S VOLUME	OLD WEIGHT	NEW WEIGHT
	DOT	DENSITY 4			
1	1.0010	1.0082	963.1	971.0	960.3
2	1.0170	1.1091	1103.3	1293.0	1172.2
3	1.0350	0.9903	1625.4	1624.0	1634.0
4	1.0510	0.9010	820.0	756.0	832.5
5	1.0000	0.9379	1032.0	1011.0	1038.2
6	1.0290	0.9761	1009.1	985.0	1014.0

THE R FOREARM DENSITY 4 MEAN VALUE IS 1.0054

Figure 36. HER1 Output.

SECTION 6

THE AEROSPACE MEDICAL RESEARCH LABORATORY DATA BANK AND RELATED MATERIALS

Since the formulation of the AMRL Data Bank, five anthropometric data tapes have been documented and published in AMRL Technical Reports, several others are near publication form, and several programs are now being prepared for publication as AMRL Technical Reports. Two publications, referenced later in this section, have been submitted which fully document four anthropometric survey data tapes, and the correlation tape which contains correlation information for seven anthropometric surveys. Also two correlation tapes of a comparison format, each containing two groups of survey data, which were prepared independent of the AMRL Data Bank are described.

6.1 THE AMRL DATA BANK LIBRARY OF COMPUTER PROGRAMS

Work is progressing steadily on the library of computer programs. A large portion of the documentation has been written and several programs await final touchup, including the XVAL and MSDP programs. Work towards completion of this library is at this time picking up speed. The programs, with complete documentation, will be published during the coming year as part of an AMRL Technical Report.

6.2 THE AMRL DATA BANK TAPE LIBRARY

The standardization of the AMRL Data Bank Tape Library is progressing steadily. Five tapes have been fully documented and published in AMRL-TR-77-2 in September 1976 (see Reference 10). The first four tape volumes in the Technical Report contain the basic survey data from the four most important USAF anthropometric surveys: the 1950 and 1967 surveys of flying personnel, the 1968 survey of Air Force Women, and the 1965 survey of male personnel. The fifth tape is the tape of U. S. correlations which is documented in Paragraph 6.3 of this report.

6.2.1 Tape Format

Since the AMRL report on these tapes is rather complete, this report will only attempt to familiarize the reader with their basic format and content. These tapes have been prepared in essentially a common format for ease in their use not only in AMRL, but in research efforts elsewhere as well. All records on the tape are in 80-character card-image form. The tapes have been made relatively self-explanatory in as much as only one format statement to read in text and other format statements contained in the tape, need be supplied by the user. Each tape contains a heading record, an identification record, a small amount of historical background information on the data, coding information, data variable names, ranges, suitable interval widths for frequency tables, conversion factors for the data, and all but one format statement for reading the tape. Several relevant constants are also provided in the third record of each tape. Figures 37a-f show a listing of the first five subjects of the 1968 USAF female personnel survey tape. The text explaining the different sections of the tape is quoted directly from AMRL-TR-77-2.

6.2.2 Summary

Since the publication of the AMRL Technical Report on the first five volumes of the Data Bank Tape library, nine other tapes are in near-standard form, lacking only historical background and coding information. These nine and several others will be completed during the next contract period.

6.3 INTERCORRELATIONS OF ANTHROPOMETRIC MEASUREMENTS

Three correlation tapes have been prepared during the past year. Two of them have been comparison oriented tapes, each containing the information from two different correlation matrices. The third tape contains eleven files of correlation matrices based on data from seven large U.S. anthropometric surveys.

REC 0001.. ** AMRL DATA BANK LIBRARY - VOLUME I - 1968 SURVEY OF AIR FORCE WOMEN **

Line 1, as it appears, is simply the name of the survey. This is repeated as the last line of the tape heading so that it can be used as a heading for any output generated by the use of this tape.

REC 0002.. (6(9M ,I4))

Line 2 is a format statement for reading in and writing out the next line.

REC 0003.. NSURVEY= 101; NVQ = 140; NVT = 156; NSB = 1905; NLS = 47; NDATE = 7608

Line 3 provides several constants relevant to the contents of the tape: NSURVEY - an identifying number for the survey; here, NSURVEY=101
 NVQ - the number of ordinal variables; NVQ=140.
 NVT - the total number of variables; NVT=156.
 (Non-ordinal variables always follow the ordinal ones.)
 NSB - the number of subjects; NSB=1905.
 NLS - the number of lines of the description of the survey and its coding; NLS=43.
 NDATE - the date at which this tape was prepared; NDATE=7608, i.e., August 1976.

REC 0004.. (I4,2X,249,3F8.2,2F6.2,2F10.7)
 REC 0005.. (I4,2X,3A6,3F8.2,2F6.2,2F10.7)
 REC 0006.. (I4,2X,4A4,A2,3F8.2,2F6.2,2F10.7)

Lines 4, 5, and 6 are three alternate formats for use in reading in the name-range-conversion constant records. The first of these reads in the name as two 9-character words, the second as three 6-character words, and the third a four 4-character and one 2-character words. The user of these tapes will presumably use the format most appropriate for his computer, or simply use the last of the three.

Figure 37a. The Heading and Identification Records and Some Formats (Reference 10).

The next several lines (i.e., NLS lines) are background material of some value, we hope, to the user of the tape's data but irrelevant to the computer's treatment of these data. The last of these NLS lines is a repeat of the initial line.

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REC 0007.. THE SURVEY OF WOMEN OF THE AIR FORCE WAS MADE IN THE SPRING OF 1968 BY THE ANTH
REC 0008.. ROPOLOGY BRANCH, AEROSPACE MEDICAL RESEARCH LABORATORY, WRIGHT-PATTERSON AFB, O
REC 0009.. HIO AND THE ANTHROPOLOGY RESEARCH PROJECT (THEN AT ANTIOCH COLLEGE, YELLOW SPRIN
REC 0010.. G3, OHIO). DATA FOR AGE (VARIABLE 1), 123 BODY SIZE MEASUREMENTS (VARIABLES 2-12
REC 0011.. 4), AND GRIP STRENGTH (VARIABLE 129) WERE OBTAINED FROM A SAMPLE OF 1909 WOMEN.
REC 0012.. 13 MEASUREMENTS WERE REPEATED ON 1513 SUBJECTS WITH THE SUBJECTS WEARING FOUNDA
REC 0013.. TION GARMENTS (VARIABLES 126-138). AGE, AGE AT MENARCHE, AND YEAR OF BIRTH (AFTE
REC 0014.. R 1900) ARE RECORDED IN TENTHS OF YEARS; YEAR OF MEASUREMENT (AFTER 1900) IN HUN
REC 0015.. DREDTHS OF YEARS. SKINFOLDS ARE RECORDED IN TENTHS OF MILLIMETERS, WEIGHT AND
REC 0016.. REPORTED WEIGHT IN POUNDS, REPORTED STATURE IN INCHES, GRIP STRENGTH IN KILOGRA
REC 0017.. MS. ALL OTHER METRIC VARIABLES WERE RECORDED IN MILLIMETERS.
REC 0018.. CODED VARIABLES----
REC 0019.. 1-AGE
REC 0020.. AS REPORTED PLUS 0.5
REC 0021.. 1-1.FOUNDATION GARMENT
REC 0022.. 1-REGULAR PANTY GIROLE / 2-LONG LEG PANTY GIROLE / 3-REGULAR GIROLE / 4-LONG
REC 0023.. LEG GIROLE / 5-CORSET / 6-PANTY / 7-MISCELLANEOUS OR NOT SPECIFIED /
REC 0024.. 1-2.AIR FORCE SPECIALTY CODE (SEE TAPE BOOKLET)
REC 0025.. 1-3.MARITAL STATUS
REC 0026.. 1-SINGLE / 2-MARRIED / 3-DIVORCED / 4-OTHER /
REC 0027.. 1-45.RANK
REC 0028.. 11-BASIC AIRMAN / 12-AIRMAN / 13-AIRMAN FIRST CLASS / 14-SERGEANT / 15-STAFF
REC 0029.. SERGEANT / 16-TECHNICAL SERGEANT / 17-MASTER SERGEANT / 18-SENIOR MASTER
REC 0030.. SERGEANT / 21-OFFICER TRAINEE / 31-20 LT / 32-1ST LT / 33-CAPTAIN / 34-MAJOR /
REC 0031.. 35-LT-COL / 36-COLONEL /
REC 0032.. 1-46.COMMAND
REC 0033.. 1-AFSC / 2-AFLC / 3-ATC / 4-SAG / 5-AOC / 6-TAC /
REC 0034.. 1-47.LOCATION
REC 0035.. 1-CARSWELL / 2-LACKLAND / 3-RANDOLPH / 4-SHEPPARD / 5-WRIGHT-PATTERSON /
REC 0036.. 6-SEWARD /
REC 0037.. 1-48.BLOOD TYPE
REC 0038.. 1-A / 2-B / 3-AB / 4-O /
REC 0039.. 1-49.RH FACTOR
REC 0040.. 1-NEG / 2-POS /
REC 0041.. 1-50.HANDEDNESS
REC 0042.. 1-RIGHT / 2-LEFT / 3-AMBIDEXTROUS /
REC 0043.. 151-153.BIRTHPLACE (SUBJECT, FATHER, AND MOTHER)
REC 0044.. 11-MAINE / 12-NEW HAMPSHIRE / 13-VERMONT / 14-MASS / 15-RHODE IS / 16-CONN / 21-NEW
REC 0045.. YORK / 22-NEW JERSEY / 23-PENNSYLVANIA / 31-DELAWARE / 32-MARYLAND / 33-DC / 34-VIRGINIA
REC 0046.. 41-OHIO / 42-INDIANA / 43-ILLINOIS / 44-MICHIGAN / 45-WISCONSIN / 51-KENTUCKY
REC 0047.. 52-TENNESSEE / 53-MISSISSIPPI / 54-ALABAMA / 61-MINNESOTA / 62-IOWA
REC 0048.. 63-MISSOURI / 64-N DAKOTA / 65-S DAKOTA / 66-NEBRASKA / 67-KANSAS / 71-ARKANSAS
REC 0049.. 72-LOUISIANA / 73-OKLAHOMA / 74-TEXAS / 81-MONTANA / 82-IDAHO / 83-WYOMING
REC 0050.. 84-COLORADO / 85-UTAH / 86-NEVADA / 87-ARIZONA / 88-N MEXICO / 91-CALIFORNIA
REC 0051.. 92-OREGON / 93-WASHINGTON / 94-ALASKA / 95-HAWAII / SEE TAPE BOOKLET FOR
REC 0052.. FOREIGN CODES. /
REC 0053.. ** AMRL DATA BANK LIBRARY - VOLUME I - 1968 SURVEY OF AIR FORCE WOMEN **

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Figure 37b. The Historical Background and Coding Information (Reference 10).

The following NVT (as read from line 3) lines provide information about each variable: names, ranges, conversion constants, and the like. This information can be ignored, in whole or part, by both the human users of these tapes and the computers. The I-th of these lines contains, in order:

$I, (Name(I,L), L=1, NLGTH), (A(I,L), L=1, 7)$

where $NLGTH$ is the length of the name in words. $NLGTH$ depends on the computer word length and must be supplied by the user of the tape.

The quantities $A(I,L)$ are these--we illustrate using the values for weight:

$A(I,1)=82.50$ a value slightly lower than the smallest value of weight recorded. This value was selected as an appropriate lower limit for the first interval when weights are grouped for frequency tables containing up to but not in excess of 50 intervals.

$A(I,2)=200.00$ the largest weight recorded.

$A(I,3)=126.00$ an approximation to the mean weight, included for use in reducing the size of summations of squares and higher powers.

$A(I,4)=3.00$ a suggested interval width for frequency tables which are limited to a maximum of 50 intervals. In this case, a table of 40 intervals will result; an interval of 2 pounds would have been too fine, and would have resulted in almost 60 intervals. Intervals for linear measurement have generally been restricted to values of 1, 2, 5, 10, 15 or 20 mm.

$A(I,5)=5.00$ a suggested interval width for frequency tables which are limited to a maximum of 30 intervals.

$A(I,6)=0.4535924$ a constant to convert the summary statistics from the units in which they were measured to the desired metric units for output. Here the conversion is from pounds to kilograms. Since the measurements are generally made in metric units, the function of $A(I,6)$ is usually to adjust the location of the decimal point.

$A(I,7)=2.2046223$ a constant to convert the metric output to English units. For weight, this constant converts from kilograms back into pounds.

Figure 37c. The Variable Name-Range Records
(Reference 10).

REC 0054..	1	AGE	10000	97500	23000	1000	2000	1000000	10000000
REC 0055..	2	HEIGHT	8250	20000	12600	300	500	4535924	22046223
REC 0056..	3	TRICEP SKINFOLD	5250	46800	18000	1000	2000	1000000	3937008
REC 0057..	4	SUBSCAPULAR SKINFOLD	4250	37200	12000	1000	2000	1000000	3937008
REC 0058..	5	SUPRAILLIAC SKINFOLD	4250	50000	19000	1000	2000	1000000	3937008
REC 0059..	6	MEDIAL CALF SKINFOLD	1250	37200	15000	1000	2000	1000000	3937008
REC 0060..	7	STATURE	144250	183000	162000	1000	2000	1000000	3937008
REC 0061..	8	STATURE, MAXIMUM	144250	184000	162000	1000	2000	1000000	3937008
REC 0062..	9	CERVICAL HEIGHT	120250	156800	139000	1000	2000	1000000	3937008
REC 0063..	10	ACROMIAL HEIGHT	114250	152000	131000	1000	2000	1000000	3937008
REC 0064..	11	SUPRASIERNAL HEIGHT	116250	150600	131000	1000	2000	1000000	3937008
REC 0065..	12	BUST POINT HEIGHT	100250	136300	119000	1000	2000	1000000	3937008
REC 0066..	13	WAIST HEIGHT	86250	115500	100000	1000	2000	1000000	3937008
REC 0067..	14	ABDOMINAL EXT HGT	78250	104000	93000	1000	2000	1000000	3937008
REC 0068..	15	TROCHANTERIC HGT	68250	96500	82000	1000	2000	1000000	3937008
REC 0069..	16	BUTTOCK HEIGHT	64250	96600	82000	1000	2000	1000000	3937008
REC 0070..	17	GLUTEAL FURROW HGT	58250	86400	72000	1000	2000	1000000	3937008
REC 0071..	18	TIBIAL HEIGHT	33250	49600	41000	500	1000	1000000	3937008
REC 0072..	19	CROTCH HEIGHT	60250	87500	74000	1000	2000	1000000	3937008
REC 0073..	20	ANKLE HEIGHT	7250	16000	11000	500	500	1000000	3937008
REC 0074..	21	LAT'L MALLEOLUS HT	4750	8700	5700	500	500	1000000	3937008
REC 0075..	22	SITTING HT, RELAXED	73250	96000	84000	500	1000	1000000	3937008
REC 0076..	23	SITTING HEIGHT	75250	96400	85500	500	1000	1000000	3937008
REC 0077..	24	EYE HEIGHT, SITTING	63250	83100	73600	500	1000	1000000	3937008
REC 0078..	25	MIDSHOULDER HT, SIT	50250	67200	57600	500	1000	1000000	3937008
REC 0079..	26	WAIST HGT, SITTING	17750	29200	23100	500	500	1000000	3937008
REC 0080..	27	ELBOW REST HEIGHT	14250	29500	22500	500	1000	1000000	3937008
REC 0081..	28	POPITEAL HEIGHT	33250	47100	40300	500	1000	1000000	3937008
REC 0082..	29	BUTTOCK-POPITEAL L	38250	58500	47600	500	1000	1000000	3937008
REC 0083..	30	BUTTOCK-KNEE LGTH	48250	66400	57200	500	1000	1000000	3937008
REC 0084..	31	ACROMION-RADIAL L	25250	36500	30900	500	500	1000000	3937008
REC 0085..	32	RADIAL-STYLION L	18750	28000	23200	500	500	1000000	3937008
REC 0086..	33	THUMB-TIP REACH	62250	87200	74000	1000	1000	1000000	3937008
REC 0087..	34	THUMB-TIP, EXTENDED	70250	100000	83000	1000	2000	1000000	3937008
REC 0088..	35	OVERHEAD REACH	174250	227600	198000	1500	3000	1000000	3937008
REC 0089..	36	NECK CIRCUMFERENCE	28250	39900	33600	500	500	1000000	3937008
REC 0090..	37	SHOULDER CIRCUMFER	86250	122100	103000	1000	2000	1000000	3937008
REC 0091..	38	CHEST CIRC AT SCYE	70250	103500	84000	1000	2000	1000000	3937008
REC 0092..	39	BUST CIRCUMFERENCE	74250	113900	89000	1000	2000	1000000	3937008
REC 0093..	40	CHEST C BELOW BUST	60250	97000	74000	1000	2000	1000000	3937008
REC 0094..	41	WAIST CIRCUMFERENCE	52250	95100	67000	1000	2000	1000000	3937008
REC 0095..	42	ABDOMINAL EXT CIRC	64250	119000	85500	1500	2500	1000000	3937008
REC 0096..	43	HIP C-7" BLM WAIST	76250	117000	93000	1000	2000	1000000	3937008
REC 0097..	44	HIP C-9" BLM WAIST	76250	120100	95000	1000	2000	1000000	3937008
REC 0098..	45	UPPER THIGH CIRCUM	42250	72000	55000	1000	2000	1000000	3937008
REC 0099..	46	KNEE CIRCUMFERENCE	30250	45700	36000	500	1000	1000000	3937008
REC 0100..	47	CALF CIRCUM, RIGHT	26250	44500	34000	500	1000	1000000	3937008
REC 0101..	48	CALF CIRCUM, LEFT	26250	44000	34000	500	1000	1000000	3937008
REC 0102..	49	ANKLE CIRCUMFERENCE	17250	25600	21000	500	500	1000000	3937008
REC 0103..	50	VERTICAL TRUNK CIRC	134250	178200	154000	1000	2000	1000000	3937008
REC 0104..	51	VERTICAL TRX C, SIT	132250	170500	150000	1000	2000	1000000	3937008
REC 0105..	52	BUTTOCK CIRC, SIT	84250	128400	99000	1000	2000	1000000	3937008
REC 0106..	53	SCYE CIRCUMFERENCE	28250	49000	37000	500	1000	1000000	3937008
REC 0107..	54	AXILLARY ARM CIRC	20250	39100	27200	500	1000	1000000	3937008
REC 0108..	55	BICEPS C, RELAXED, R	19250	37400	25200	500	1000	1000000	3937008
REC 0109..	56	BICEPS C, FLEXED, R	19250	39000	25400	500	1000	1000000	3937008
REC 0110..	57	BICEPS C, RELAXED, L	19250	37800	25600	500	1000	1000000	3937008
REC 0111..	58	BICEPS C, FLEXED, L	19250	39200	25400	500	1000	1000000	3937008
REC 0112..	59	ELBOW CIRC, FLEXED	21250	35800	26700	500	1000	1000000	3937008
REC 0113..	60	FOREARM C, RELAXED	19250	30000	23400	500	500	1000000	3937008
REC 0114..	61	FOREARM C, FLEXED	19250	32800	24900	500	1000	1000000	3937008
REC 0115..	62	WRIST CIRCUMFERENCE	12250	17600	14800	500	500	1000000	3937008
REC 0116..	63	BIACROMIAL BREADTH	30750	41600	35700	500	500	1000000	3937008
REC 0117..	64	BIDELTOID BREADTH	34250	50100	41700	500	1000	1000000	3937008
REC 0118..	65	CHEST BREADTH	22250	35900	27900	500	1000	1000000	3937008
REC 0119..	66	BUST PT-BUST PT BR	12750	24600	18300	500	500	1000000	3937008
REC 0120..	67	WAIST BREADTH	18250	32700	24000	500	1000	1000000	3937008
REC 0121..	68	HIP BREADTH	28250	44100	34800	500	1000	1000000	3937008
REC 0122..	69	THIGH-THIGH BR, SIT	23250	50200	38000	500	1000	1000000	3937008
REC 0123..	70	HUMERAL BREADTH, R	5150	7500	6100	100	100	1000000	3937008

Figure 37d. (Reference 10).

REC 0124..	71	HUMERAL BREADTH, L	5150	7400	5100	100	100	1000000	3937008
REC 0125..	72	FEMORAL BREADTH, R	6650	9900	8100	200	200	1000000	3937008
REC 0126..	73	FEMORAL BREADTH, L	6650	9900	8100	200	200	1000000	3937008
REC 0127..	74	CHEST DEPTH	18250	32300	23400	500	1000	1000000	3937008
REC 0128..	75	WAIST DEPTH	12250	25500	18800	500	1000	1000000	3937008
REC 0129..	76	ABDOMINAL EXT DPTH	15250	30300	20700	500	1000	1000000	3937008
REC 0130..	77	BUTTOCK DEPTH	15250	30600	21000	500	1000	1000000	3937008
REC 0131..	78	THIGH CLEARANCE	8750	16900	12400	500	500	1000000	3937008
REC 0132..	79	SHOULDER LENGTH	11250	18800	14600	500	500	1000000	3937008
REC 0133..	80	NECK-BUST POINT L	19250	32000	25200	500	1000	1000000	3937008
REC 0134..	81	STRAP LENGTH	52250	79700	65000	1000	2000	1000000	3937008
REC 0135..	82	INTERSCYE	27250	44200	34800	500	1000	1000000	3937008
REC 0136..	83	INTERSCYE, MAXIMUM	37250	60500	49000	500	1000	1000000	3937008
REC 0137..	84	BACK CURVATURE	33250	53500	42400	500	1000	1000000	3937008
REC 0138..	85	WAIST BACK	33250	48100	40500	500	1000	1000000	3937008
REC 0139..	86	ANTERIOR WAIST LTH	27250	41500	33300	500	1000	1000000	3937008
REC 0140..	87	SLEEVE INSEAM	36250	53500	44000	500	1000	1000000	3937008
REC 0141..	88	SPINE-TO-SCYE LGTH	15250	25500	20100	500	500	1000000	3937008
REC 0142..	89	SPINE-TO-ELBOW LTH	44250	62500	53200	500	1000	1000000	3937008
REC 0143..	90	SPINE-TO-WRIST LTH	67250	91200	79500	500	1000	1000000	3937008
REC 0144..	91	HAND LENGTH	15250	22000	18200	200	500	1000000	3937008
REC 0145..	92	HAND BREADTH	6450	8800	7500	100	200	1000000	3937008
REC 0146..	93	HAND CIRCUMFERENCE	14750	21500	18200	500	500	1000000	3937008
REC 0147..	94	FOOT LENGTH	20750	27600	24000	500	500	1000000	3937008
REC 0148..	95	FOOT BREADTH	6750	11000	8800	500	500	1000000	3937008
REC 0149..	96	HEAD LENGTH	16250	20700	18400	200	200	1000000	3937008
REC 0150..	97	HEAD BREADTH	12250	17100	14500	200	200	1000000	3937008
REC 0151..	98	HEAD CIRCUMFERENCE	49750	61700	54600	500	500	1000000	3937008
REC 0152..	99	TRAGION-TO-HEAD	10250	16100	12600	200	500	1000000	3937008
REC 0153..	100	ECTOCANTHUS-TO-NOSE	8250	15700	11600	200	500	1000000	3937008
REC 0154..	101	PROMASALE-TO-HEAD	10250	19300	14600	200	500	1000000	3937008
REC 0155..	102	SUBNASALE-TO-HEAD	12250	20500	15800	200	500	1000000	3937008
REC 0156..	103	STOMION-TO-HEAD	14250	23100	17800	200	500	1000000	3937008
REC 0157..	104	MENTON-TO-HEAD	18250	26800	21800	200	500	1000000	3937008
REC 0158..	105	TRAGION-TO-WALL	7250	14600	10000	200	500	1000000	3937008
REC 0159..	106	ECTOCANTHUS-WALL	13250	21200	16200	200	500	1000000	3937008
REC 0160..	107	PROMASALE-TO-WALL	13250	25000	21000	200	500	1000000	3937008
REC 0161..	108	SUBNASALE-TO-WALL	16250	24000	19600	200	500	1000000	3937008
REC 0162..	109	LIP PROTRUSION-WALL	16250	24100	19200	200	500	1000000	3937008
REC 0163..	110	MENTON-TO-WALL	14250	22900	18200	200	500	1000000	3937008
REC 0164..	111	SAGITTAL CURVATURE	29750	41500	34500	500	500	1000000	3937008
REC 0165..	112	BITRACION-CORONAL	29750	39200	33900	500	500	1000000	3937008
REC 0166..	113	BICULAR BREADTH	7850	11200	9600	200	200	1000000	3937008
REC 0167..	114	BIAURICULAR BREADTH	13250	20100	15800	200	500	1000000	3937008
REC 0168..	115	BITRACION BREADTH	11250	15200	12800	200	200	1000000	3937008
REC 0169..	116	BIZYGOMATIC BREADTH	10850	14900	12800	200	200	1000000	3937008
REC 0170..	117	BIZYGOMATIC BREADTH	8650	12200	10100	200	200	1000000	3937008
REC 0171..	118	NASAL BREADTH	2250	4600	3100	200	200	1000000	3937008
REC 0172..	119	LIP LENGTH	3650	5800	4300	200	200	1000000	3937008
REC 0173..	120	MENTON-SUBNASALE L	3850	7500	5500	100	200	1000000	3937008
REC 0174..	121	MENTON-SELLION LTH	4650	12800	10600	100	200	1000000	3937008
REC 0175..	122	SUBNASALE-SELLION	3050	6100	4500	100	200	1000000	3937008
REC 0176..	123	EAR LENGTH	3450	6900	5200	100	200	1000000	3937008
REC 0177..	124	EAR BREADTH	1850	4200	2900	100	200	1000000	3937008
REC 0178..	125	GRIP STRENGTH	950	5300	2900	100	200	1000000	3937008
REC 0179..	126	WAIST HEIGHT, OFG	86250	115300	100000	1000	2000	1000000	3937008
REC 0180..	127	ABDOM EXT HGT, OFG	78250	107900	92000	1000	2000	1000000	3937008
REC 0181..	128	WAIST CIRCUM, OFG	54250	89000	66000	1000	2000	1000000	3937008
REC 0182..	129	ABDOM EXT CIRC, OFG	64250	118200	87000	1500	2500	1000000	3937008
REC 0183..	130	HIP C-7" BLW M, OFG	76250	118800	93000	1000	2000	1000000	3937008
REC 0184..	131	HIP C-9" BLW M, OFG	76250	120200	95000	1000	2000	1000000	3937008
REC 0185..	132	WAIST BREADTH, OFG	17250	30800	21300	500	1000	1000000	3937008
REC 0186..	133	HIP BREADTH, OFG	27250	42700	33600	500	1000	1000000	3937008
REC 0187..	134	WAIST DEPTH, OFG	11250	24700	15600	500	1000	1000000	3937008
REC 0188..	135	ABDOM EXT DPTH, OFG	13250	30200	19600	500	1000	1000000	3937008
REC 0189..	136	BUTTOCK DEPTH, OFG	16250	30400	21300	500	1000	1000000	3937008
REC 0190..	137	BUTTOCK C, SIT, OFG	82250	128800	99000	1000	2000	1000000	3937008
REC 0191..	138	THI-THI 3R, SIT, OFG	28250	48300	37200	500	1000	1000000	3937008
REC 0192..	139	STATURE REPORTED	5750	7400	5400	100	100	25400250	3937008
REC 0193..	140	WEIGHT REPORTED	8150	19500	12000	500	500	4535924	22046223

Figure 37e. (Reference 10).

REC 0194..	141	FOUNDATION GARMENT	50	900	300	100	100	10000000	10000000
REC 0195..	142	AFSC	8750	9912830	5558000	98500396500	10000000	10000000	10000000
REC 0196..	143	RACE	50	300	200	100	100	10000000	10000000
REC 0197..	144	MARITAL STATUS	50	400	100	100	100	10000000	10000000
REC 0198..	145	RANK (NUMERICAL)	1050	3600	1700	100	200	10000000	10000000
REC 0199..	146	COMMAND	50	600	200	100	100	10000000	10000000
REC 0200..	147	LOCATION	50	600	200	100	100	10000000	10000000
REC 0201..	148	BLOOD TYPE	50	400	200	100	100	10000000	10000000
REC 0202..	149	RH FACTOR	50	200	100	100	100	10000000	10000000
REC 0203..	150	HANDINESS	50	300	100	100	100	10000000	10000000
REC 0204..	151	BIRTHPLACE,SUBJECT	-50	10000	4000	1000	1000	10000000	10000000
REC 0205..	152	BIRTHPLACE,FATHER	-50	10000	4000	1000	1000	10000000	10000000
REC 0206..	153	BIRTHPLACE,MOTHER	-50	10000	4000	1000	1000	10000000	10000000
REC 0207..	154	YEAR OF BIRTH	-11500	50500	50500	1000	1000	10000000	10000000
REC 0208..	155	AGE AT MENARCHE	8500	20800	13000	500	500	10000000	10000000
REC 0209..	156	YEAR MEASURED	3900	9200	4500	100	100	10000000	10000000
REC 0210..	(14.19F4.0/2120F4.0/),2125F3.0,F5.0/1,20F4.0/9F4.0,F3.0,F6.0,8F2.0,5F3.0,F4.0)								

At the end of the list of name-range-conversion unit records is the format statement for reading in the data. While the data were written on the tape in integer format to save space, the format statement provided assumes that everything except the subject number is to be treated as floating decimal values. This format statement is, therefore, not suitable for listing data read from the tape.

This material is followed by the data. Each data record consisting of a subject number (increasing but not always consecutive) followed by NVT data values. The last data record is followed by a pseudo-data record for which the subject number is negative. Thus the user can read in all the data by reading the data for NSB subjects or by reading data until a negative subject number is sensed. Care should be taken in reading the data until an end of file (EOF) is sensed to insure that the pseudo-data record is not treated as a normal data record.

REC 0211..	1	285	112	124	78	86	1501967198111315126912511130	928	058	778	763	675	406	703
REC 0212..	120	85	835	855	722	573	234	204	389	459	536	308	238	729
REC 0213..	749	642	848	882	897	524	357	326	330	21115061474	945	343	252	228
REC 0214..	22122814836139227619123333382	62	62	86	8525318322719912014325764934862425	376								
REC 0215..	339439192532802169	74	179230	86183162565140122152163182223106166209195195188	392									
REC 0216..	372	95	169	133	126	97	35	43	95	109	50	96	32	25
REC 0217..	214	328	177	223	215	922	357	62	116	2	9754	2	132	2
REC 0218..	2	315	127	182	106	108	1081624164114061310132711791000	937	830	800	764	405	738	
REC 0219..	113	60	850	873	769	603	261	255	397	476	585	307	235	745
REC 0220..	741	669	829	943	986	508	358	338	332	196161215271050	391	279	251	267
REC 0221..	225237146360409288194239395412	55	55	80	80254170204239142164270657352471195	419								
REC 0222..	343434214541805175	76171230	8618514453912117133146166209110171218202202184	355										
REC 0223..	325	94	166	125	111	93	33	46	57	106	51	53	34	32
REC 0224..	228	358	168	204	244	986	399	64	122	2	9754	2	232	2
REC 0225..	3	455	126	160	164	326	68162216301379129613001169	968	887	857	795	705	406	731
REC 0226..	125	68	887	899	788	588	220	223	394	441	548	310	237	737
REC 0227..	811	747	900	925	930	925	390	331	195161715571011	191	295	265	270	266
REC 0228..	242252155379420329177275333376	62	60	76	75251183218188120159279714385950451	420								
REC 0229..	359432221556818184	81	02242	87184150593122111140150167205101164210196194184	373									
REC 0230..	351	97	160	132	130	111	12	42	54	106	46	60	35	33
REC 0231..	260	335	185	221	216	995	362	64	126	3	9735	2	135	2
REC 0232..	4	295	143	352	192	456	352161416191370129412931171	971	876	819	771	684	385	731
REC 0233..	103	65	883	896	790	615	254	275	390	450	578	291	220	658
REC 0234..	760	782	905	9701045	598	396	355	366	230164515641095	344	304	298	304	294
REC 0235..	263275160360407300198251382423	63	62	85	87254183220233142155259662330504394	415								
REC 0236..	357410201522765174	73183233	86181152573130111140148165209124183223213208200	345										
REC 0237..	370	105	165	129	135	112	28	43	60	115	50	50	36	24
REC 0238..	0	0	0	0	0	0	0	65	144	7	9754	2	232	2
REC 0239..	5	235	146	180	110	132	1701703170714421375138612331037	950	866	954	777	461	794	
REC 0240..	127	77	876	901	784	614	261	235	433	475	605	327	240	754
REC 0241..	779	782	890	9591000	593	385	364	359	220183415661038	380	286	274	291	271
REC 0242..	243266155373437297182255355388	65	63	87	8625217121723315516227669735553400	411								
REC 0243..	363467205937812193	80193249	92196152580139133167179260228105170221203195183	383										
REC 0244..	336	98	176	133	126	95	28	48	60	114	50	97	25	371058
REC 0245..	230	357	177	242	2531013	392	68	145	4	9754	2	232	2	5

Figure 37f. The Subject Data Format and the Data Itself for the First Five Subjects (Reference 10).

6.3.1 Two Tapes for Comparison

The first two correlation tapes contain information from the 1968 USAF WOMEN survey versus 1967 USAF MEN survey, and from the 1965 USAF survey's black basic trainees versus white basic trainees. One hundred similar variables from the three surveys were chosen by Edmund Churchill of Webb Associates for the basis of these tapes. The first two records on the tape are 80-character card images and contain the formats needed for reading the tape. Header information is contained in the next three records which describe the layout of the variable names and statistical information. Original survey variable names are listed for each survey along with their survey numbers (SR NO), mean values for each variables (X-BAR), and standard deviations (SD). Both surveys are listed side-by-side, as shown in Figure 38, with the two right-most columns listing the arithmetic differences between X-BAR (DELTA XBAR) and SD(DELTA SD) for the two surveys for each variable. Following the variable names is a table, which is 22 card-image records long, which illustrates the layout of the correlations. The correlations for both surveys are listed in one 100X 100 element matrix. The diagonal elements of the matrix were all set to zero while the correlations of one survey occupy the upper right section of the matrix and those for the second survey the lower left section of the matrix. Figure 38 is a partial printout of the 1967 USAF MEN versus 1968 USAF WOMEN (WAF) tape. Thus far no analyses have been done using these two tapes.

6.3.2 U.S. Correlations

The third correlation tape of correlation matrices was documented and published in September 1976 in AMRL-TR-77-1 (see Reference 11). The following is a portion of the abstract from that publication.

"Correlation matrices based on data from USAF anthropometric surveys of women (1968, 125 variables), flying personnel (1950, 128 variables; 1967, 190 variables), and basic trainees (1965, 161 variables); a U.S. Army survey of women separatees (1946, 60 variables); the Health Examination

(0A10,/,2(13A10,/,1,100(2(21A,2X,2A9,2F11.5,5X),2F11.5),22(,/,)
(16F8.5)

THE 1967 USAF AND WAF CORRELATION FILE

		MAF		1967 USAF		SD		DELTA		DELTA	
SR NO	NAME	X-BAR	SD	SR NO	NAME	X-BAR	SD	X-BAR	SD	X-BAR	SD
1	AGE	22.92756	6.45104	1	AGE	30.02802	6.29563	-7.10126	.15621	-7.10126	.15621
2	WEIGHT	127.28189	16.56658	2	WEIGHT	173.57594	21.41646	-46.29405	-4.02988	-46.29405	-4.02988
3	TRICEPS SKINFOLD	190.32441	54.41558	3	SKF TRICEPS-LANGE	123.74211	5.13204	177.58230	49.28354	177.58230	49.28354
4	SURSCAPULAR SKINFOLD	128.59108	49.47769	4	SKF SURSCAP-R-LNGE	135.65639	5.33002	111.92469	33.14747	111.92469	33.14747
5	SURAILIAC SKINFOLD	197.23465	70.12367	5	SKF SUPRAILIAC-HPN	242.16197	103.36749	-44.92732	-33.24782	-44.92732	-33.24782
6	STATURE	1621.03307	60.03850	11	HEIGHT (STATURE)	1773.53049	61.73432	-152.49742	-1.69582	-152.49742	-1.69582
7	CERVICAL HEIGHT	1391.95748	55.19079	14	CERVICAL HEIGHT	1520.74547	58.12487	-128.78799	-2.93409	-128.78799	-2.93409
8	ACROMIAL HEIGHT	1318.60053	54.79437	15	ACROMIAL HEIGHT	1452.19394	57.48096	-133.59341	-2.68659	-133.59341	-2.68659
9	SUPRASTERNAL HEIGHT	1320.01365	53.01809	19	SUPRASTERNAL HEIGHT	1452.04416	54.91285	-132.03051	-1.89996	-132.03051	-1.89996
10	BUST POINT HEIGHT	1193.18793	52.13736	20	NIPPLE HEIGHT	1292.59108	52.24976	-109.40315	-1.1240	-109.40315	-1.1240
11	MAIST HEIGHT	1062.78740	44.98502	21	MAIST HT-OMPHALION	1064.82542	47.11151	-62.03842	-2.12649	-62.03842	-2.12649
12	TROCHANTERIC HEIGHT	826.72441	42.67776	24	TROCHANTERIC HEIGHT	939.69036	43.46657	-112.96595	-2.78831	-112.96595	-2.78831
13	BUTTOCK HEIGHT	822.12703	41.62904	23	BUTTOCK HEIGHT	911.19520	43.83550	-79.06816	-2.20846	-79.06816	-2.20846
14	GLUTEAL FURROW HGT	727.00840	39.61141	25	GLUTEAL FURROW HGT	811.27908	40.04570	-84.26968	-1.43478	-84.26968	-1.43478
15	TRIALE HEIGHT	419.82467	23.76293	25	KNEE CIRC HEIGHT	496.48001	24.85706	-76.65534	-1.09413	-76.65534	-1.09413
16	CROTCH HEIGHT	745.04409	40.29395	26	CROTCH HEIGHT	850.82288	41.44373	-105.77879	-1.14978	-105.77879	-1.14978
17	ANKLE HEIGHT	111.86719	13.54234	31	ANKLE HEIGHT	137.18763	11.48895	-25.32044	2.05339	-25.32044	2.05339
18	LAT'L MALLEOLUS HT	67.73858	5.87042	132	LAT'L MALLEOLUS HT	70.39802	5.42078	-2.66024	.44964	-2.66024	.44964
19	SITTING HEIGHT	855.99948	31.68807	32	SITTING HEIGHT	931.82709	31.70558	-75.82761	-0.1750	-75.82761	-0.1750
20	EYE HEIGHT SITTING	737.04462	30.50081	33	EYE HEIGHT SITTING	809.47833	30.12741	-72.43371	.45340	-72.43371	.45340
21	HDSHOULDER HT, SIT	579.97638	26.58103	34	HDSHOULDER HT/SIT	645.93774	27.40611	-65.96136	-1.82598	-65.96136	-1.82598
22	ELBOW REST HEIGHT	227.06142	24.61921	36	ELBOW REST HGT/SIT	251.63904	26.07191	-24.57762	-1.45870	-24.57762	-1.45870
23	POPLITEAL HEIGHT	410.47454	18.60513	38	POPLITEAL HGT/SIT	437.07404	22.40403	-26.59950	-1.79891	-26.59950	-1.79891
24	POPLITEAL HEIGHT	477.10709	27.58567	40	POPLITEAL HGT/SIT	503.83045	25.73078	-26.73136	1.85489	-26.73136	1.85489
25	BUTTOCK-KNEE LNTH	574.28137	26.33893	39	BUTTOCK-KNEE LNTH	604.12157	26.97580	-29.84021	-1.63647	-29.84021	-1.63647
30	ACROMION-RADIALE L	310.05932	16.25687	43	ACROMION-RADIALE L	329.47244	17.00262	-19.41312	-1.74575	-19.41312	-1.74575
32	RADIALE-STYLION L	233.86667	13.68019	45	RADIALE-STYLION LH	268.83635	14.20863	-34.96948	-1.52845	-34.96948	-1.52845
33	THUMB-TIP REACH	741.11234	38.76264	47	THUMB-TIP REACH	803.15986	39.75051	-61.84752	-1.98787	-61.84752	-1.98787
34	THUMB-TIP, EXTENDED	830.33176	48.77919	48	THUMB-TIP R"CH/XTD	895.94194	45.15364	-57.61018	3.62554	-57.61018	3.62554
36	NECK CIRCUMFERENCE	337.49334	16.76671	66	NECK CIRC - MAXIMUM	393.42486	19.12700	-45.93062	-2.36829	-45.93062	-2.36829
37	SHOULDER CIRCUMFER	1004.12703	51.38271	67	SHOULDER CIRCUM"CE	1176.91249	58.07640	-172.78546	-6.69369	-172.78546	-6.69369
39	CHEST CIRC AT SCYE	842.48976	49.63574	68	CHEST CIRC AT SCYE	1022.47917	69.56740	-179.98941	-10.93185	-179.98941	-10.93185
41	MAIST CIRCUMFERENCE	672.03202	54.76665	70	MAIST CIRC-OMPHAL"N	875.95456	73.67513	-203.92254	-18.90828	-203.92254	-18.90828
43	UPPER THIGH CIRCUM	554.75381	42.19422	96	UPPER THIGH CIRCUM	588.15113	44.32350	-33.39332	-2.12928	-33.39332	-2.12928
46	KNEE CIRCUMFERENCE	763.01470	22.46598	98	KNEE CIRCUMFERENCE	786.74716	22.74432	-23.73246	1.91015	-23.73246	1.91015
47	CALF CIRCUM, RIGHT	341.43573	22.46598	100	CALF CIRCUM"CE	371.91418	22.73158	-30.47848	-2.65680	-30.47848	-2.65680
49	ANKLE CIRCUMFERENCE	210.85039	12.88973	102	ANKLE CIRCUM"CE	224.10012	12.64359	-13.24973	.24614	-13.24973	.24614
50	VERTICAL TRUNK CIR	1544.26299	68.69045	74	VERTICAL TRUNK CIR	1680.66849	71.57992	-136.40550	-2.88588	-136.40550	-2.88588
51	BUTTOCK CIRC, SIT	999.97323	60.86607	73	BUTTOCK CIRCUM/SIT	1076.30121	69.43687	-112.39904	-3.87533	-112.39904	-3.87533
52	SCYE CIRCUMFERENCE	370.97848	22.86439	103	SCYE CIRCUMFERENCE	403.60959	27.76742	-112.63111	-8.88243	-112.63111	-8.88243
53	TRICEPS C-RELAXED, R	256.11391	22.93311	104	TRICEPS C-EXTEND/RT	307.81321	23.34424	-51.69930	.41113	-51.69930	.41113
54	TRICEPS C-FLXED, R	267.94016	23.15454	106	TRICEPS C-FLXED/RT	327.41691	22.57789	-59.47675	.57866	-59.47675	.57866
55	ELBOW CIRC, FLEXED	269.76430	17.82707	109	ELBOW CIRC-C-FLEXED	312.39293	17.45950	-42.62863	.36756	-42.62863	.36756
59	FOREARM C, RELAXED	234.76374	13.78454	110	FOREARM C-EXTEND	291.52797	14.61580	-46.76419	-1.83126	-46.76419	-1.83126
61	FOREARM C, FLEXED	249.75066	15.19692	111	FOREARM C-FLEXED	297.67396	15.80570	-47.92330	-1.60978	-47.92330	-1.60978

Figure 38. Listing of Correlation Tape of 1967 USAF Men Vs. 1968 USAF Women (WAF) for 100 Variables.
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62	47	WRIST CIRCUMFERENCE	1-9.62520	7.11526	112	47	WRIST CIRCUMFERENCE	175.46832	9.22987	-26.24312	-2.11461
63	48	BIACROMIAL BREADTH	758.43307	16.39323	50	48	BIACROMIAL BREADTH	407.27724	19.43351	-48.84417	-3.02028
64	49	BIDELTIOID BREADTH	418.73648	23.13384	51	49	BIDELTIOID BREADTH	492.35759	25.61348	-63.62111	-2.47964
65	50	CHEST BREADTH	279.94908	19.14410	52	50	CHEST BREADTH	327.83929	21.20119	-47.89021	-2.05799
66	51	MAIST BREADTH	241.27979	19.35696	53	51	MAIST BREADTH-OMPH"	309.50645	23.82195	-68.30666	-4.46499
67	52	HIP BREADTH	349.68504	22.16016	55	52	HIP BREADTH	352.63063	18.83757	-2.94559	3.12259
68	53	HUMERAL BREADTH, R	61.37596	3.06809	57	53	ELBOW BREADTH BONE/R	92.62793	3.61485	-9.49198	-1.54686
69	54	FEMORAL BREADTH, R	81.16430	4.51149	60	54	BUTTOCK CIRCUMFERENCE	986.11274	55.03811	-904.94444	-50.52662
70	55	MAIST DEPTH	170.14435	16.71806	63	55	MAIST DEPTH-OMPH"	233.00463	21.79307	-52.86027	-5.07598
71	56	BUTTOCK DEPTH	211.53333	17.98843	64	56	SCROTAL-A MAIST/S	254.35423	16.98753	-42.82089	-9.1090
72	57	THIGH CLEAFANCE	124.36273	12.52023	65	57	SCROTAL-SUPRASTERNLE	698.40586	34.11433	-564.12313	-21.59410
73	58	SHOULDER LENGTH	146.60787	10.21260	118	58	SHOULDER LENGTH	166.03618	12.60748	-19.42810	-2.39488
74	59	INTERSCYE	353.57165	24.40531	120	59	INTERSCYE	397.48043	37.62551	-36.90878	-13.22021
75	60	INTERSCYE, MAXIMUM	493.94341	32.86887	121	60	INTERSCYE	615.39629	30.17511	-121.49288	2.69376
76	61	MAIST BACK	405.11181	22.15890	124	61	MAIST BACK-OMPHL"	489.16870	23.74216	-64.05689	-1.58326
77	62	SLEEVE INSLAM	441.27192	24.15305	49	62	SCRTL-MAIST/BUIT/S	395.20993	29.17263	-46.06199	-5.01959
78	63	SPINE-TO-SCYE LGTH	203.66142	13.57075	113	63	SLVE L/SPINE-SCYE	284.50904	18.10506	-80.84763	-4.53431
79	64	SPINE-TO-ELBOW LTH	533.17218	24.06219	114	64	SLVE L/SPINE-ELBOW	605.77997	26.16635	-72.60779	-2.10417
80	65	SPINE-TO-WRIST LTH	795.83832	33.18881	115	65	SLVE L/SPINE-WRIST	908.19562	35.1134	-112.35710	-1.99253
81	66	HAND LENGTH	183.83202	9.59008	134	66	HAND LENGTH	191.08666	8.19930	-7.25464	1.39078
82	67	HAND BREADTH	75.54121	3.89407	136	67	HAND C/METACARPAL	89.01052	4.14629	-13.46931	-2.25222
83	68	WRIST CIRCUMFERENCE	103.18005	9.07175	138	68	HAND C/METACARPAL	215.53008	9.38321	-32.35003	-7.31146
84	69	FOOT LENGTH	240.68609	11.27779	125	69	FOOT LENGTH	270.34118	11.89037	-29.65599	-6.1258
85	70	FOOT BREADTH	88.67612	4.37733	127	70	FOOT BREADTH	97.66260	4.94664	-8.98648	-0.3074
86	71	HEAD LENGTH	184.10184	6.78907	150	71	HEAD LENGTH	198.70088	6.74496	-14.59905	-0.4411
87	72	HEAD BREADTH	145.15433	5.94739	156	72	HEAD BREADTH	155.98612	5.41646	-10.83179	-5.3093
88	73	HEAD CIRCUMFERENCE	548.65459	16.23607	141	73	HEAD CIRCUMFERENCE	575.14724	14.25937	-26.49265	1.97670
89	74	TRAGION-TO-HEAD	127.25144	7.64118	180	74	TRAGION-TO-VERTEX	134.44131	6.09917	-7.18907	1.54202
90	75	ECTOCANTHUS-TO-HEAD	117.84777	5.16908	175	75	XTNRL CANTHUS-VRTX	119.49853	7.70147	-1.85076	1.48761
91	76	PRONASALE-TO-HEAD	147.60525	11.71497	176	76	PRONASALE-TO-VRTX	177.42238	11.02870	-1.8287	1.8287
92	77	SUBNASALE-TO-HEAD	159.12389	10.97692	177	77	SUBNASALE-TO-VRTX	150.87842	10.26629	-1.75453	7.1063
93	78	STATION-TO-HEAD	178.26194	11.21225	174	78	STATION-TO-VERTEX	131.64114	10.00654	-5.37920	1.20571
94	79	MENTON-TO-HEAD	219.87034	11.59334	179	79	MENTON-TO-VERTEX	227.70509	10.24193	-8.63475	1.15141
95	80	TRAGION TO WALL	101.72441	8.99934	188	80	TRAGION-TO-WALL	103.35339	6.48766	-14.21363	2.51158
96	81	ECTOCANTHUS-WALL	163.65722	9.66342	183	81	XTNRL CANTHUS-WALL	177.87084	6.59513	-14.21363	3.08829
97	82	PRONASALE TO WALL	211.88871	9.60781	184	82	PRONASALE-TO-WALL	226.78797	7.49986	-14.89925	2.10795
98	83	SUBNASALE TO WALL	196.62415	9.81356	185	83	SUBNASALE-TO-WALL	209.90366	7.83880	-13.27951	1.97476
99	84	LIP PROTRUSION-WALL	193.81102	10.26511	186	84	LIP PROTRUSION-WALL	211.81296	8.59613	-18.60193	2.02898
100	85	MENTON TO WALL	182.33333	11.36097	187	85	CHIN PROMINENCE-WALL	204.72865	10.46713	-22.39532	1.40970
101	86	SAGITTAL CURVATURE	347.85984	14.88556	142	86	SAGITTAL ARC/INION	346.45015	16.54723	1.40970	-1.66167
102	87	TRAGION-CORONAL	339.22257	14.04592	144	87	TRAGION-CORONAL	357.55953	12.60126	-18.33696	1.44467
103	88	BICULAR BREADTH	96.72756	4.91864	162	88	BICULAR BREADTH	91.70593	4.84959	-5.02163	0.06905
104	89	STAGIRICULAR BREADTH	158.33543	9.49797	161	89	EAR-TO-EAR BREADTH	188.30837	8.07816	-29.97294	1.41981
105	90	TRAGION BREADTH	128.89239	4.96695	158	90	TRAGION BREADTH	142.51914	5.5189	-13.62675	-1.55294
106	91	TRIGONOMIC BREADTH	129.39108	5.78027	159	91	TRIGONOMIC BREADTH	142.24651	5.14941	-13.25545	6.2086
107	92	BICONIAL BREADTH	101.86352	5.62440	160	92	BICONIAL BREADTH	117.70332	6.91508	-15.43981	-1.29068
108	93	NASAL BREADTH	31.94278	3.29979	165	93	NOSE BREADTH	52.42280	2.93433	-3.48002	0.36636
109	94	LIP LENGTH	43.78478	4.21083	166	94	LIP LENGTH	52.29617	3.74275	-8.51139	4.6808
110	95	MENTON-SUBNASALE L	55.41207	5.02339	171	95	MENTON-SUBNASALE L	99.00210	5.26796	-13.59003	-1.16557
111	96	MENTON-SELLION LTH	106.29556	6.12060	172	96	MENTON-NASAL ROOT	120.11679	6.08862	-14.03122	0.3198
112	97	SUBNASALE-SELLION	45.46324	4.10213	168	97	SUBNASALE-NASAL RT	51.34287	3.72202	-5.87463	0.3811
113	98	EAR LENGTH	22.36799	4.27974	154	98	EAR LENGTH	65.96929	4.25970	-13.60131	0.17904
114	99	EAR BREADTH	29.61207	3.73019	153	99	EAR BREADTH	37.97350	3.01304	-8.16142	0.31715
115	100	GRIP STRENGTH	29.89106	5.70287	12	100	GRIP STRENGTH	56.40429	7.59344	-26.51243	-1.89057

Figure 38 (Continued)

WAF(1,1)	WAF(1,2)	WAF(1,3)	...	WAF(1,100)
USF(2,1)	WAF(2,2)	WAF(2,3)	...	WAF(2,100)
USF(3,1)	USF(3,2)	WAF(3,3)	...	WAF(3,100)
USF(99,1)	...USF(99,98)	WAF(99,99)	...	WAF(99,100)
USF(100,1)	...USF(100,99)	USF(100,99)	...	WAF(100,100)

Figure 38 (Continued)

Survey of civilian adults (1960-1962, 20 variables); and a survey of law enforcement officers (1974, 23 variables) are presented for the use by engineers who need them in solving design problems and by anthropologists and statisticians, whose analyses and understanding of the interrelationships of body size data depend significantly on these coefficients. Sample sizes in these surveys ranged from 2000 upward...."

Ten correlation matrices are included on the tape, four from the Health Examination Survey of civilian adults and one each from the remaining six surveys. Matrices were produced one at a time on separate tapes and then merged into one eleven-file tape. The first file is a table of contents and includes a routine for abstracting data from the tape. Paul Kikta of UDRI is directly responsible for the programming runs needed to produce the matrices and the final tape, as well as the table of confidence limits included in AMRL-TR-77-1.

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